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The Influence of Test Colors on the Color Rendering Index Maximization in a Three Component Spectral Power Distribution

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THE INFLUENCE OF TEST COLORS ON THE COLOR RENDERING INDEX
MAXIMIZATION IN A THREE COMPONENT SPECTRAL POWER DISTRIBUTION

GREGORY R. MILLER

JUNE 1976

Submitted in partial fulfillment of the requirement for the Bachelor of Science degree in Photographic Science and Instrumentation at the Rochester Institute of Technology.

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ABSTRACT

This thesis describes the technique of principle component analysis as applied to determining if a combination of three characteristic vectors would account for an underlying structure in the eight color test objects specified by the CIE for calculation of the color rendering index (CRI). Anticipated was that three vectors would account for 100 % of the variance in the eight test objects; however it was determined that three vectors account for only 96 % of the variance.

Since the analysis of the reflectance functions showed no dependence within the functions a 3^3 factorial experiment was conducted. Its purpose was to determine if the point of maximization of CRI in a three component spectral power distribution would be at 610, 540, and 450 nm when using metameric gray objects. This was postulated by Mr. Thornton in his paper "Luminosity and the Color Rendering Capability of White Light". The analysis of the resulting response surface indicated that the maximization point was not the same but if a valid point exists it lies outside the experimental boundaries of the experiment.

INTRODUCTION

Color in a perceived sense is determined by four factors, the spectral power distribution of the illuminating source, the spectral reflectance function of the object, the surround, and the human visual response. A general expression for the effect of the illuminant on a set of perceived object colors in comparison with the perceived color under a reference illuminant is provided by the color rendering index (CRI). Adopted in 1964 by the International Commission on Illumination (CIE) was the CIE Method of Measuring and Specifying Color Rendering Properties of Light Sources.¹ Use of this method produces a color rendering index, R, which is based on the amount of colorimetric shift of a set of test object colors under a reference illuminant in comparison to their color under a test illuminant of identical or nearly identical chromaticity. Agreed upon in this standard is that the CIE method be considered fundamental for appraising the color rendering properties of light sources and be recommended for design and testing of lamps.

In the paper "Luminosity and the Color Rendering Capability of White Light" it was shown that when luminosity and CRI were used as criteria, some optimized white light spectral power distribution (SPD) would significantly improve the light.² The study concluded that an additive combination of three spectral lines near 450, 540, and 610 nm approximated the white light SPD necessary to maximize luminous efficiency and CRI. The maximum CRI of a three component lamp with

a correlated color temperature of 6800 K and the CIE illuminant C as a reference was 80. Subsequent papers have shown an improvement of this figure to 94 when the three component distribution was combined with a continuous spectrum.³

Many questions have arisen concerning the adequateness of the original CIE set of eight color test samples for measurement of the general CRI. Nayatani et. al. showed that because of deficiencies in the number and choice of the test samples involved it is possible to derive, for a given reference illuminant, an infinite number of test illuminants with a different SPD that all have perfect color rendering indices.⁴ In agreeing with this view Dr. Wyszecki, of the National Research Council of Canada, has suggested the use of metameric gray object colors generated statistically so as to be non-linearly related in assessing the color matching properties of lamps.^{5,6} Nayatani and Takahama have confirmed the effectiveness of using the twelve metameric grays derived by Dr. Wyszecki in making an assessment of this type.⁷

Although the use of properly chosen line spectra can provide a wide gamut of colors these same spectra could be disastrous in reproducing certain colors. Since the CRI was shown to increase even more when combined SPDs were used it would be beneficial to know if the maximum of the three line spectra could be accounted for by an interrelationship in the test samples. If the samples are interrelated and can be represented by three functions it is highly probable that these three functions would be the cause of maximization of CRI at wavelengths of 450, 540, and 610 nm. Determination of the

existence of any mathematical relationship among the eight CIE test objects is the intent of Phase I of this research.

In Phase II the research has two possible paths. Mr. Thornton postulated that regardless of the type of test objects used the CRI would maximize at the wavelengths he had determined. Should the test objects prove to be non interrelated the metameric grays would be used in a factorial experimental design to determine if the CRI maximization occurs at the same point. The second path would be if the test objects prove to be related, the factorial experiment would then be aimed at determining a point of maximization.

COLORIMETRIC MEASUREMENT

Prior to any discussion of color rendering index one must be familiar with the procedures involved in the measurement and specification of color. Current specification in the CIE colorimetric system involves calculation of the X,Y,Z tristimulus values. To account for the human visual response the color matching functions for the CIE 1931 standard observer are used. When the standard observer views an illumination source the tristimulus values are given by:

$$X = k \sum P_{\lambda} \bar{x}_{\lambda}$$

$$Y = k \sum P_{\lambda} \bar{y}_{\lambda}$$

$$Z = k \sum P_{\lambda} \bar{z}_{\lambda}$$

where P_{λ} is the spectral distribution of the source and $\bar{x}_{\lambda}, \bar{y}_{\lambda}, \bar{z}_{\lambda}$ are the color matching functions for the standard observer. The normalization constant k is usually chosen so that the resultant value of Y is 100.00.

An object color is similarly specified by:

$$X = k \sum p_{\lambda} H_{\lambda} \bar{x}_{\lambda}$$

$$Y = k \sum p_{\lambda} H_{\lambda} \bar{y}_{\lambda}$$

$$Z = k \sum p_{\lambda} H_{\lambda} \bar{z}_{\lambda}$$

where p_{λ} is the spectral reflectance of the object, H_{λ} is the spectral distribution of the illumination source. When using the 1931 CIE standard observer the normalization constant for object

colors is defined by:

$$k = \frac{100}{\sum H_{\lambda} \bar{y}_{\lambda}}$$

These tristimulus values lead directly to the x,y,z chromaticity coordinates which are related through the following equations:

$$x = \frac{X}{X + Y + Z}$$

$$y = \frac{Y}{X + Y + Z}$$

$$z = \frac{Z}{X + Y + Z}$$

In order to provide a representation of the color diagram which is more perceptually uniform than the x,y diagram a transformation is made to the CIE 1960 UCS diagram by the following equations:

$$u = \frac{4X}{X + 15Y + 3Z} = \frac{4x}{-2x + 12y + 3}$$

$$v = \frac{6Y}{X + 15Y + 3Z} = \frac{6y}{-2x + 12y + 3}$$

$$W = 25Y^{1/3} - 17$$

COLOR RENDERING INDEX

In accordance with the CIE specification for the measurement of CRI the calculations were performed in this research using the following steps:

1) CALCULATION OF CIE 1931 TRISTIMULUS VALUES

Using spectroradiometric measurements of the test and reference illuminants with the spectral reflectances of the test objects, the CIE 1931 tristimulus values X, Y, Z and the chromaticity coordinates x, y of the illuminants and the test objects under each illuminant are calculated.

2) CIE 1960 UCS TRANSFORMATION

The CIE 1931 tristimulus values are transformed to the CIE 1960 UCS coordinates. If the test and reference illuminants are not of identical chromaticities, as is the case in this research, a transformation would be required to account for the adaptive color shift under the two illuminants.

3) CIE 1964 UNIFORM COLOR SPACE TRANSFORMATION

The u, v coordinates are transformed to the UCS system by the following formulas:

$$\begin{aligned} W_{r,i}^* &= 25(Y_{r,i})^{1/3} - 17 & W_{k,i}^* &= 25(Y_{k,i})^{1/3} - 17 \\ U_{r,i}^* &= 13W_{r,i}^*(u_{r,i} - u_r) & U_{k,i}^* &= 13W_{k,i}^*(u_{k,i} - u_k) \\ V_{r,i}^* &= 13W_{r,i}^*(v_{r,i} - v_r) & V_{k,i}^* &= 13W_{k,i}^*(v_{k,i} - v_k) \end{aligned}$$

where the subscripts r and k represent the reference and test illuminants respectively and the subscript i represents a test object color.

4) COLOR SHIFT

The color shift due to the two illuminants is given by:

$$\Delta E_i = (U_{r,i}^* - U_{k,i}^*)^2 + (V_{r,i}^* - V_{k,i}^*)^2 + (W_{r,i}^* - W_{k,i}^*)^2$$

5) COLOR RENDERING INDEX

The color rendering index is calculated from the ΔE_i as follows:

$$R_i = 100 - 4.6 \Delta E_i$$

This results in a scaling such that 100 represents a reproduction that is equal to the reference and a value of 50 represents the CRI of a standard warm white fluorescent tube. The actual value of CRI is calculated as the arithmetic average of the R_i s of the test colors used.

EVALUATION PROGRAM

Vector Analysis

The method of characteristic vector analysis is ideally suited to the determination of a mathematical relationship among the eight color test objects specified by the CIE. In this case each function is treated as a vector with 95 variables being over the wavelength range of 360 - 830 nm. This method will determine if a linear combination of three characteristic vectors will account for all the variance among the eight test object colors. The hypothesis is that three vectors will account for all variance and therefore would have some relationship to the point of maximization of CRI at 450, 540, and 610 nm. The mathematical detail and an example are given in Appendix A along with the computer program documentation.

FACTORIAL EXPERIMENT

In order to answer the question of where the CRI maximizes with a set of metameric gray object colors it is necessary to generate a response surface or equation for the dependent variable, CRI, as a function of the independent variables, in this case wavelength bands. Since the CRI reportedly maximizes at 450, 540, and 610 nm these three wavelengths were chosen as the central treatment combination of a 3 factorial experimental design. That is to say three wavelengths in each of three regions. A wavelength range of ± 10 nm from each center point was assumed which resulted in 27 unique combinations of the three

factors. Using CIE illuminant C as the reference the power levels at each combination must be calculated so as to match the tristimulus values of Illuminant C. This can be accomplished using a set of linear equations.

$$P_{\lambda 1} \bar{x}_{\lambda 1} + P_{\lambda 2} \bar{x}_{\lambda 2} + P_{\lambda 3} \bar{x}_{\lambda 3} = 98.0716$$

$$P_{\lambda 1} \bar{y}_{\lambda 1} + P_{\lambda 2} \bar{y}_{\lambda 2} + P_{\lambda 3} \bar{y}_{\lambda 3} = 100.0000$$

$$P_{\lambda 1} \bar{z}_{\lambda 1} + P_{\lambda 2} \bar{z}_{\lambda 2} + P_{\lambda 3} \bar{z}_{\lambda 3} = 118.2253$$

where $\lambda 1$, $\lambda 2$, and $\lambda 3$ are the three wavelengths in the treatment combination and $\bar{x}, \bar{y}, \bar{z}$ are the spectral tristimulus values of the CIE 1931 standard observer. The constants are the tristimulus values of CIE Illuminant C with the CIE 1931 standard observer. The calculated power levels represent the power required at each wavelength in order to match the tristimulus values and chromaticity coordinates of CIE Illuminant C.

A regression analysis on the factorial experimental data will provide the desired equation of response, CRI as a function of the input wavelengths over the region bounded by the experiment. Taking the partial derivatives with respect to the CRI for each variable and setting them equal to zero will result in the computation of a point on the response surface that is either a maximum or minimum. The second partial will indicate whether we have a maximum or minimum.

EXPERIMENTAL RESULTS

REFLECTANCE FUNCTION INTERDEPENDENCE

The CIE reflectance functions specified for use in the CRI calculation are given in Appendix B, Table 1. These reflectances were analysed using the characteristic vector analysis program in Appendix A. If the hypothesis that some combination of three unknown functions would account for the variance in the eight object colors then 100 % of the variance or trace of the variance-covariance matrix would have to be accounted for by three characteristic vectors. The results of these analyses given in Table 1 clearly indicate that three vectors account for only 96 % of the variance regardless of the base of the input data. That is either density or reflectance. These three vectors are illustrated in Figure 1. Figures 2 to 9 illustrate the real reflectance functions and the reconstructed reflectance functions based on the three characteristic vectors. Clearly with only 96 % of the variance accounted for the hypothesis must be rejected. Tables of the characteristic vectors, scalar multipliers, actual reflectance functions, the 3 and 7 component reconstructed functions and their associated errors are in Appendix B.

FACTORIAL EXPERIMENT

The results of the vector analysis indicated that the eight CIE/CRI test object colors were not interrelated. Therefore the three factorial experiment was aimed at determining if the CRI, as determined by the twelve metameric gray objects, maximized

COMPONENT	EIGENVALUE	REFLECTANCE		EIGENVALUE	DENSITY	
		PCT. TRACE	CUM. PCT.		PCT. TRACE	CUM. PCT.
1	10.1515	66.9711	66.9711	95.7453	57.8507	57.8507
2	3.6879	24.3297	91.3009	54.0957	32.6854	90.5361
3	.8392	5.5362	96.8370	9.2875	5.6116	96.1478
4	.3641	2.4022	99.2392	5.6802	3.4321	99.5798
5	.0748	.4937	99.7328	.4480	.2707	99.8505
6	.0276	.1819	99.9147	.1704	.1030	99.9534
7	.0129	.0849	99.9996	.0761	.0460	99.9994

COMPONENTS FROM THE CHARACTERISTIC VECTOR ANALYSIS OF THE
STANDARD CIE/CRI REFLECTANCE FUNCTIONS

TABLE 1

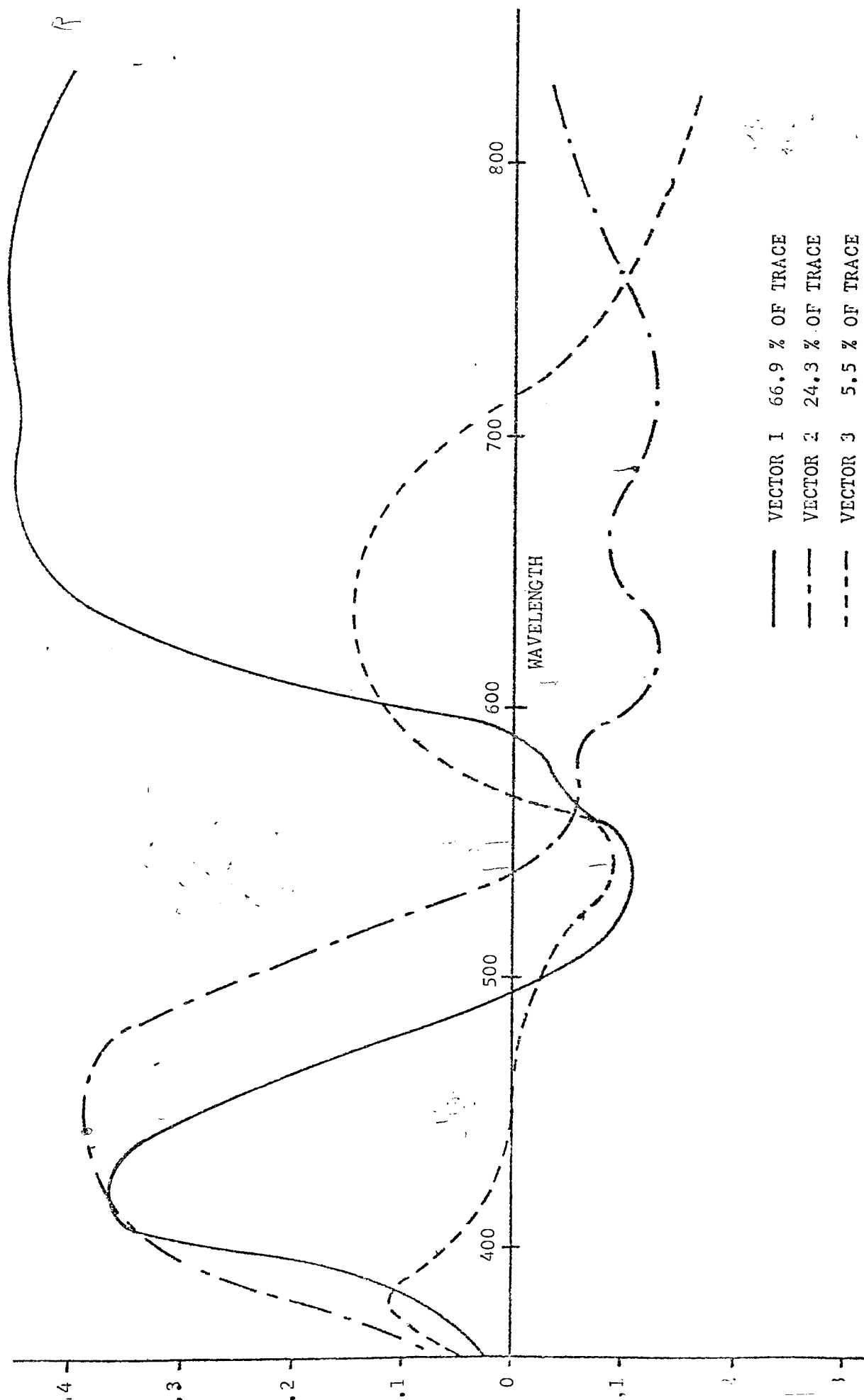


FIGURE 1

COLOR RENDERING INDEX TEST CHIP 1

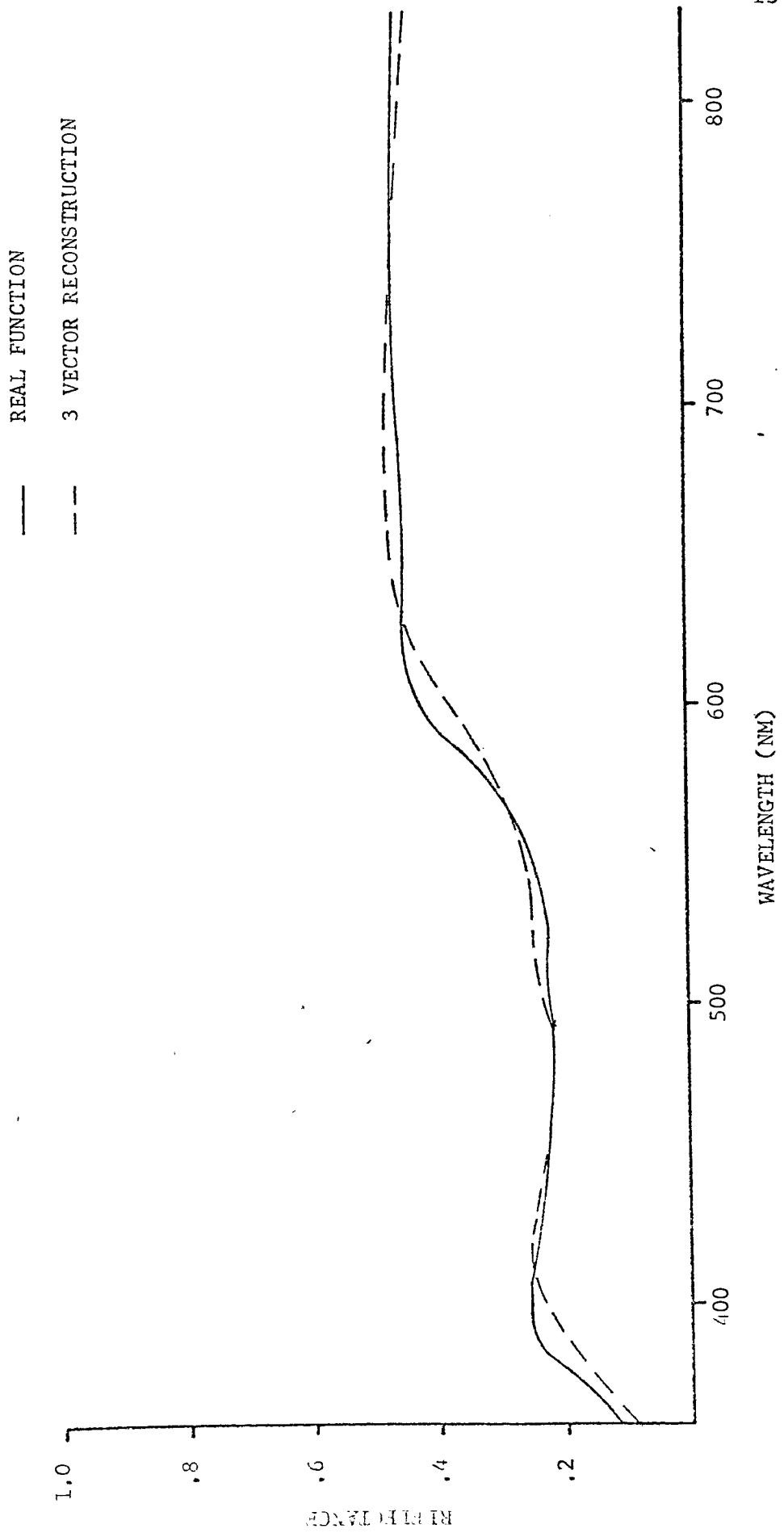


FIGURE 2

COLOR RENDERING INDEX TEST CHIP 2

— REAL FUNCTION
-- 3 VECTOR RECONSTRUCTION



FIGURE 3

COLOR RENDERING INDEX TEST CHIP 3

— REAL FUNCTION
- - 3 VECTOR RECONSTRUCTION

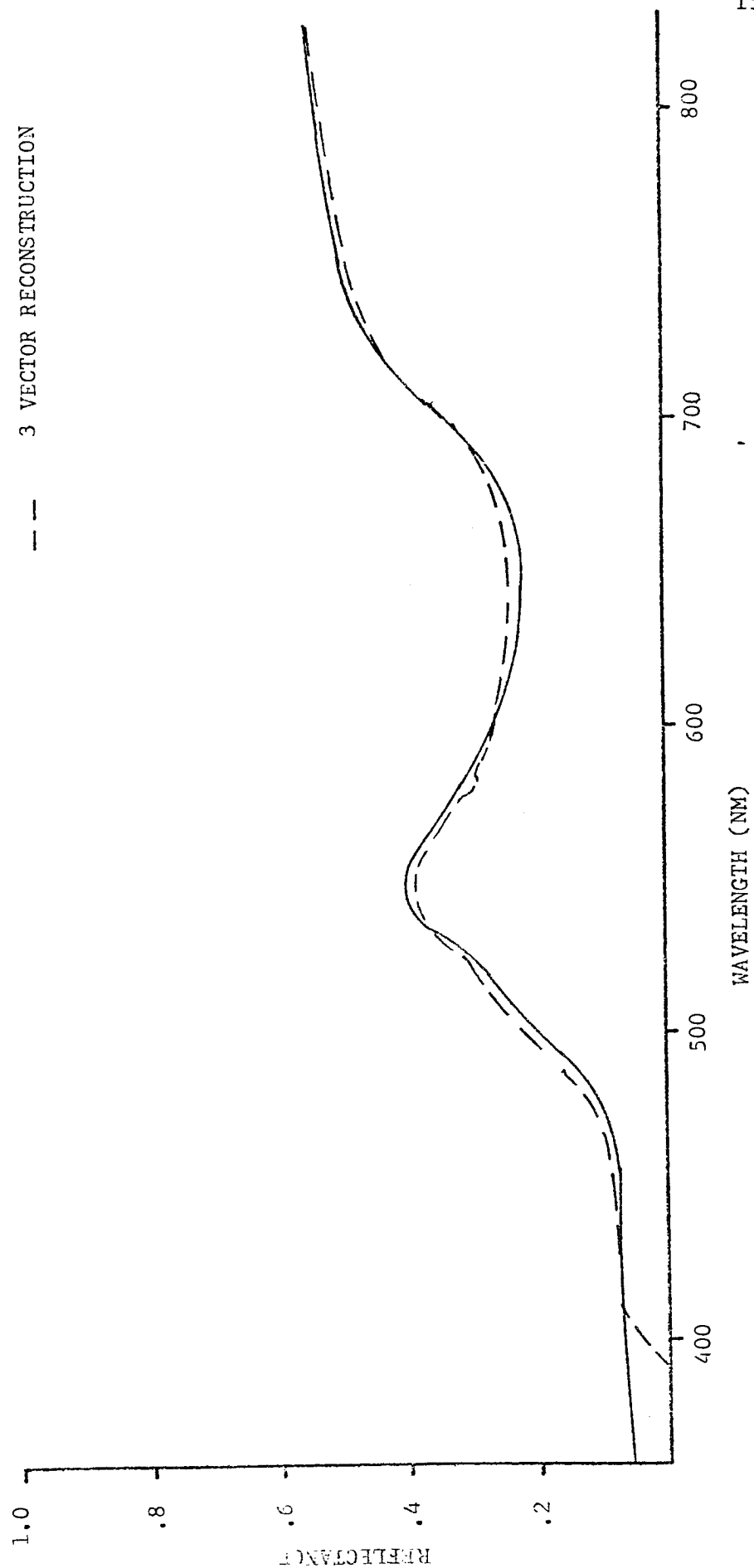


FIGURE 4

COLOR RENDERING INDEX TEST CHIP 4

— REAL FUNCTION
-- 3 VECTOR RECONSTRUCTION

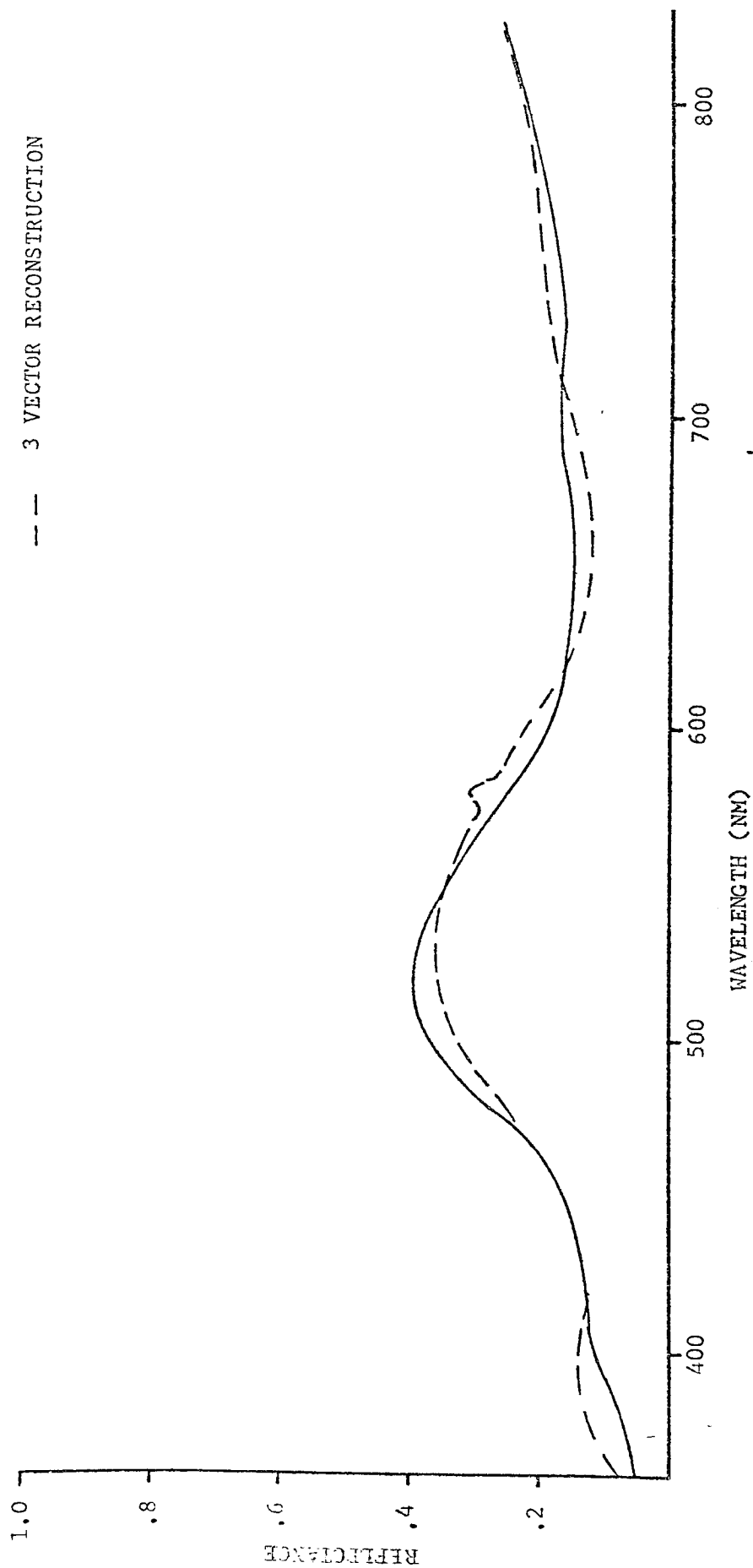


FIGURE 5

COLOR RENDERING INDEX TEST CHIP 5

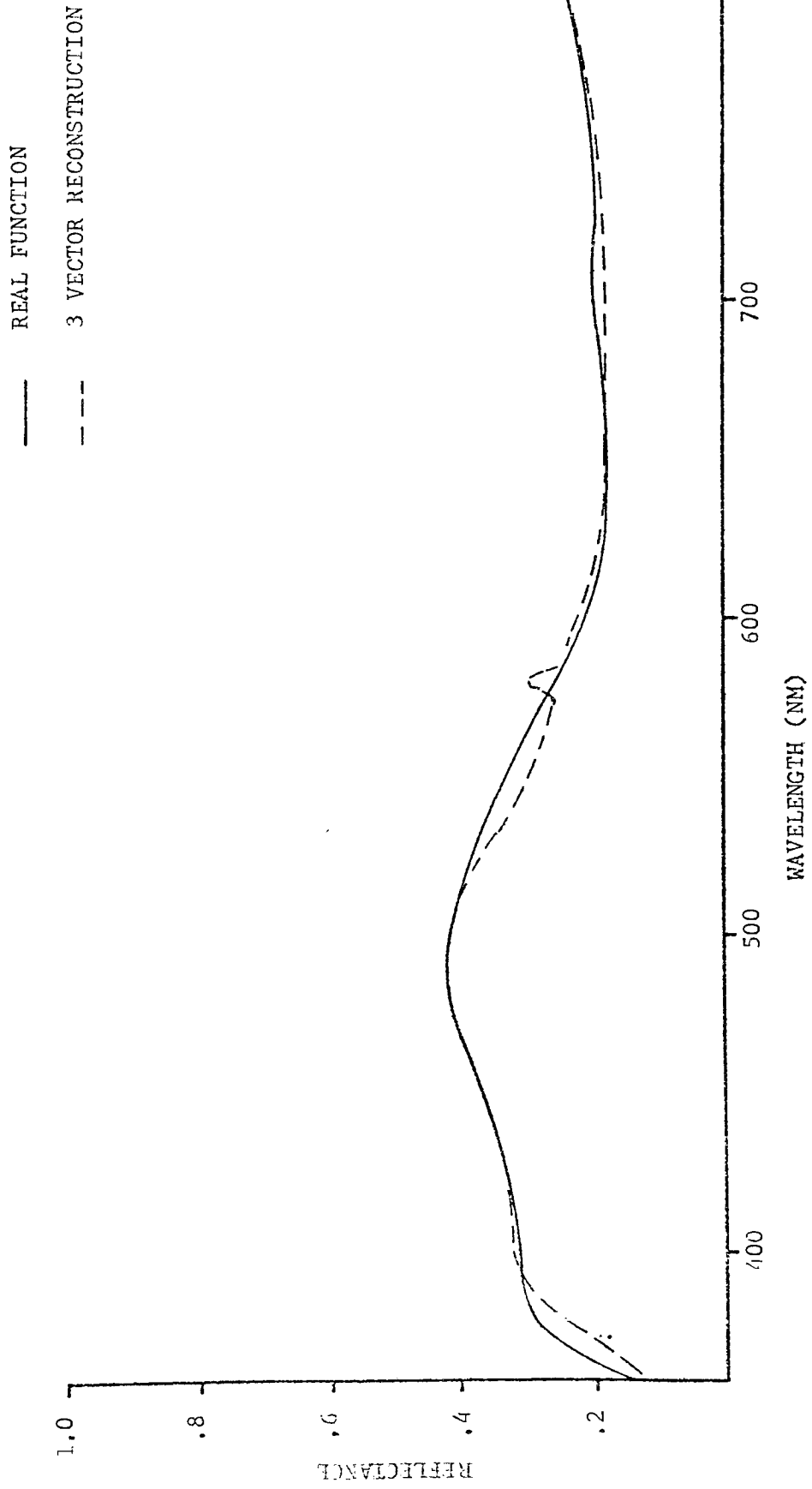
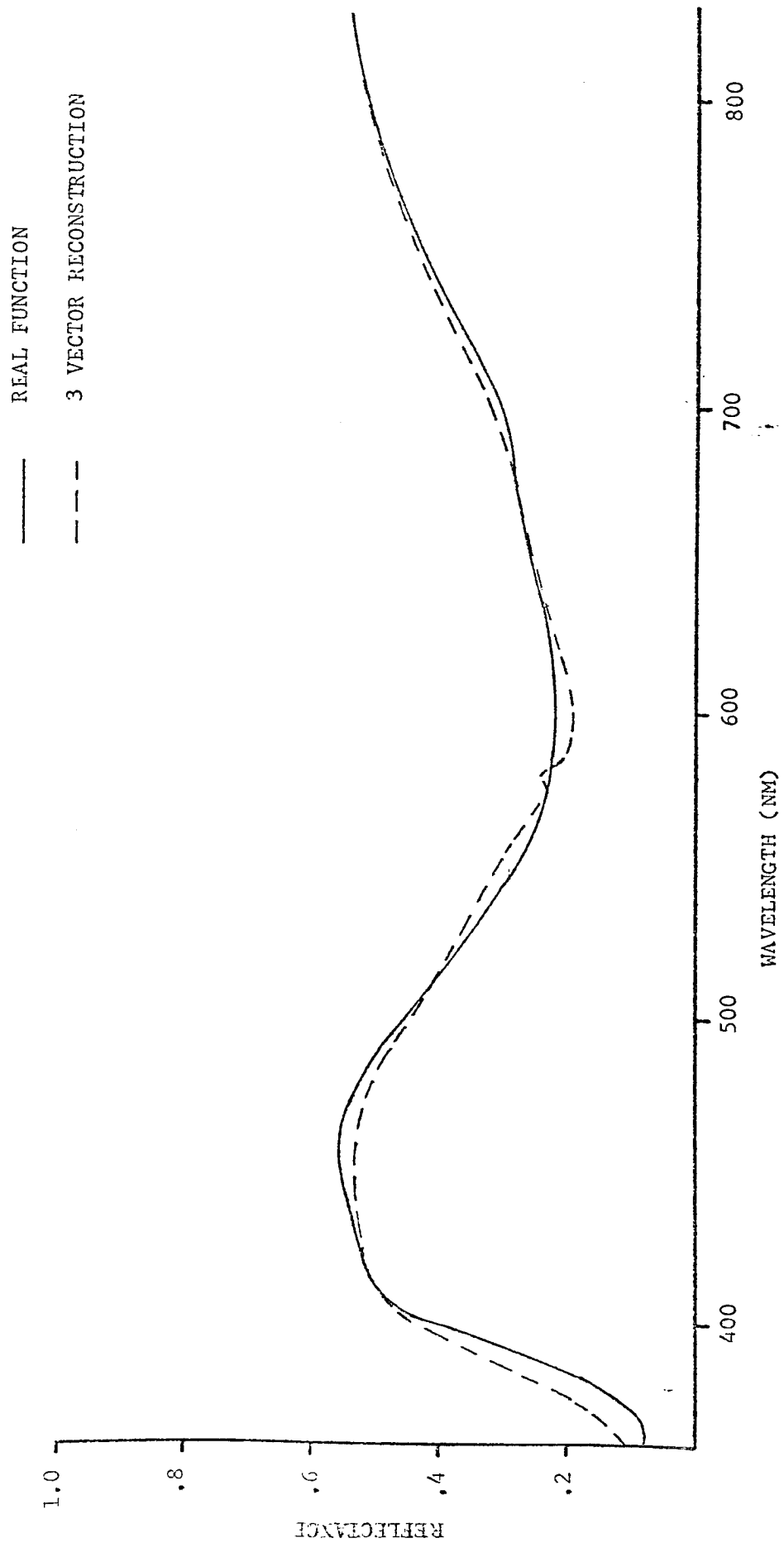


FIGURE 6

COLOR RENDERING INDEX TEST CHIP 6



COLOR RENDERING INDEX TEST CHIP 7

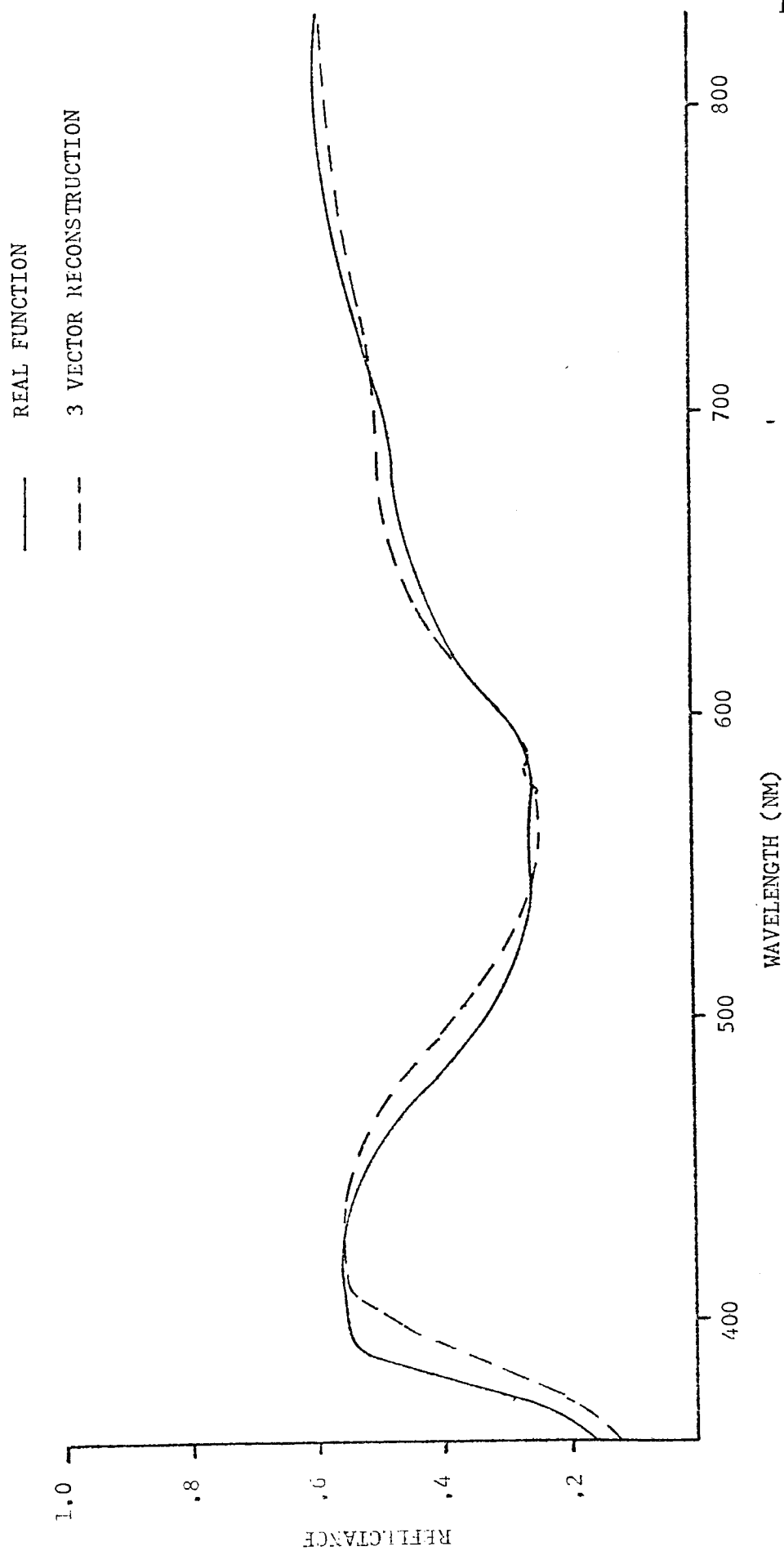
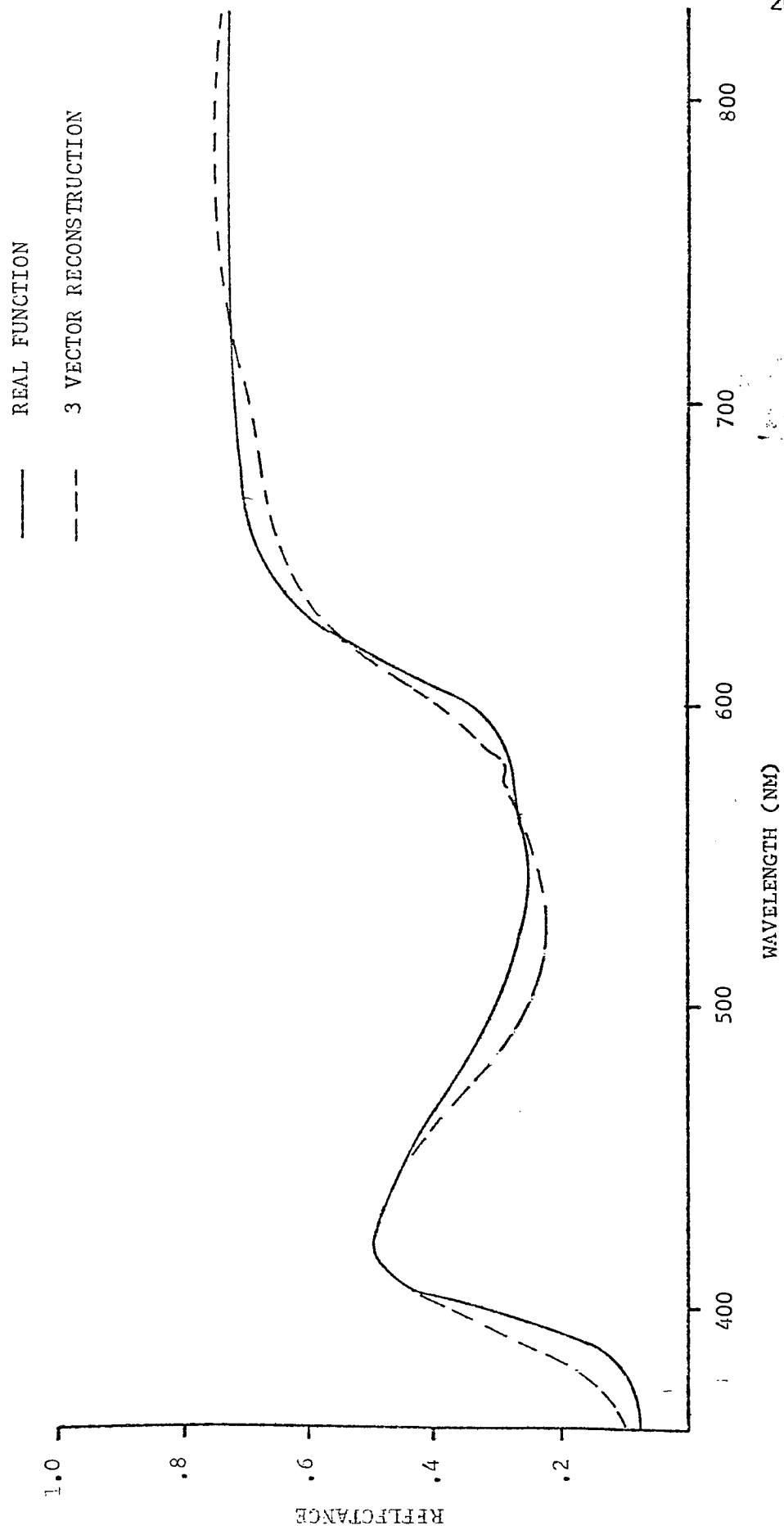


FIGURE 8

COLOR RENDERING INDEX TEST CHIP 8



AVERAGE OF COLOR RENDERING INDEX TEST CHIPS 1 - 8

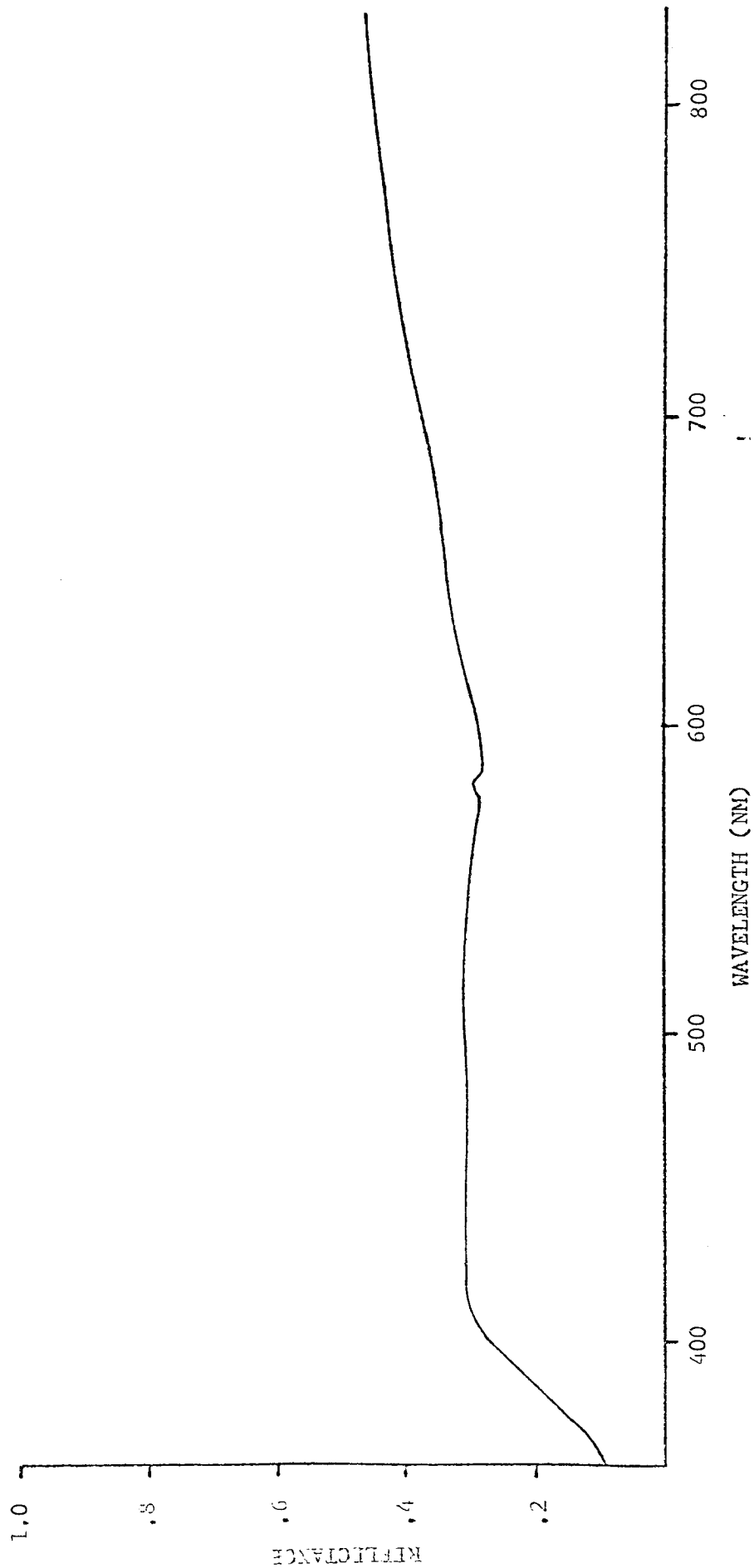


FIGURE 10

at the same wavelengths as Mr. Thornton had postulated. That is the value maximizes at the same point regardless of the choice of test object colors. As the first step the power levels for each of the wavelength combinations were calculated based on the previously given equations and are given in Table 2. These were used as test illuminants in calculation the CRI using the twelve metameric gray objects. The numerical results of these calculations are presented in Table 3. Since the CRI is scaled based on a value of 50 being that of a standard warm white florescent tube and because the color difference of the metameric functions when viewed under the line spectra in this experiment are so great the resulting values of CRI are negative. An illustration of where these object colors fall on the CIE diagram at the maximum point of CRI in the 3^3 factorial experiment is in Figure 11.

In order to determine if the maximum was at the same point the CRI data in Table 3 was placed through a regression analysis program from the Statistical Package for the Social Sciences.⁸ The resulting equation was:

$$\begin{aligned} \text{CRI} = & -22.95 + 7.95C_1 + 13.40C_2 + 5.00C_3 + 10.06C_1^2 - 20.57C_2^2 \\ & - 6.20C_3^2 - 7.54C_1C_2 - 8.94C_2C_3 \end{aligned}$$

Where C_1, C_2, C_3 are the treatment codes for Factors 1 to 3. This equation has an R square maximum of .992 while maintaining a standard error of 2.07. Using this equation and holding C_1 at a constant, lines of constant response at each level of factor C_1 were calculated and plotted in Figures 12 - 14. From these curves and Table 3 it is clear that the CRI value at the treatment combination 0,0,0 or 610, 540, 450 nm is clearly less than the CRI from 620, 540, 450 which is the best CRI under the experimental conditions. If a maximization

METAMERIC GRAY OBJECTS UNDER THREE
COMPONENT SPD (620, 540, 450 NM)

FIGURE 11

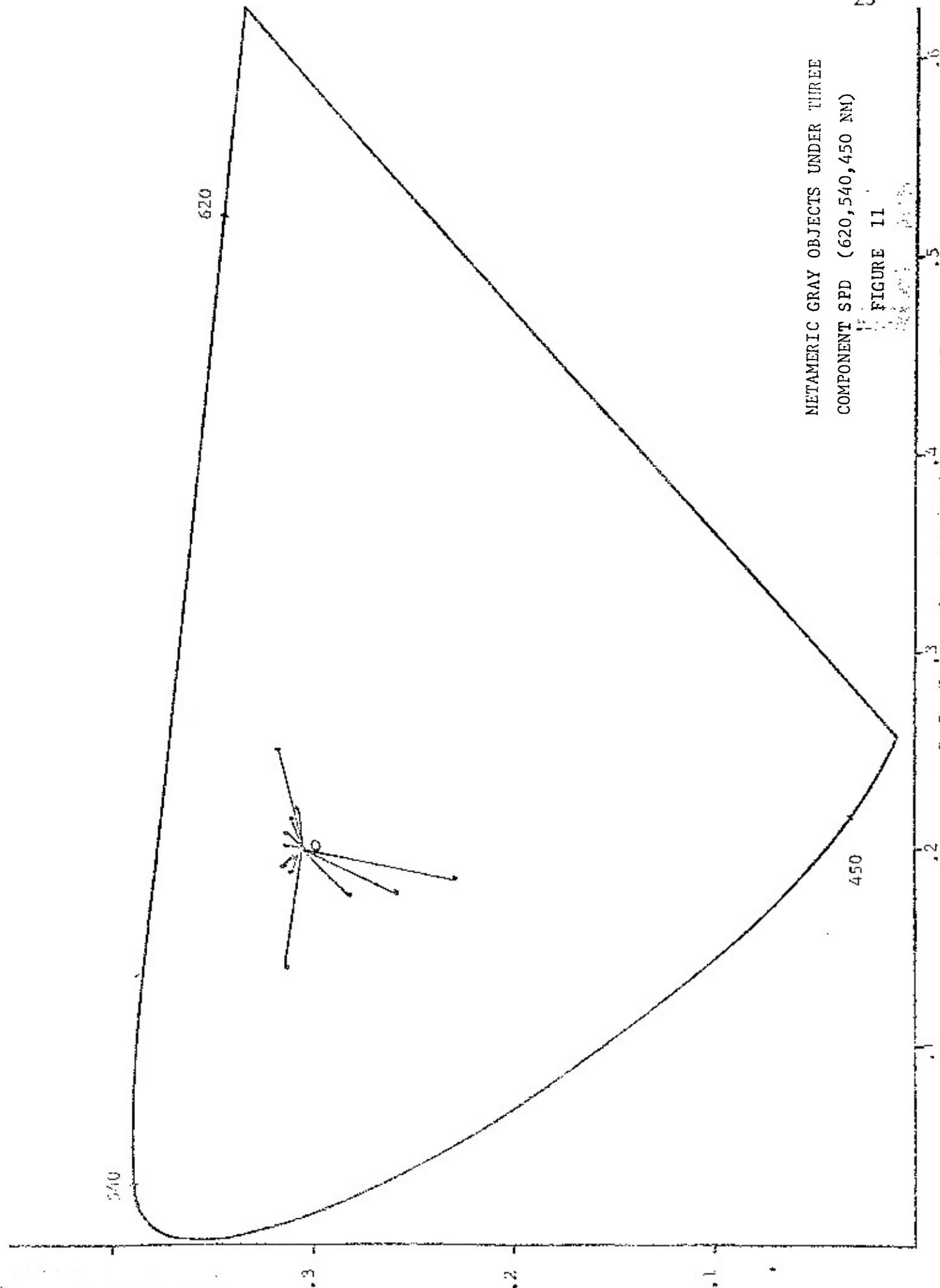


FIGURE 12
LINES OF CONSTANT RESPONSE
 $C_1 = 1$ (620 NM)

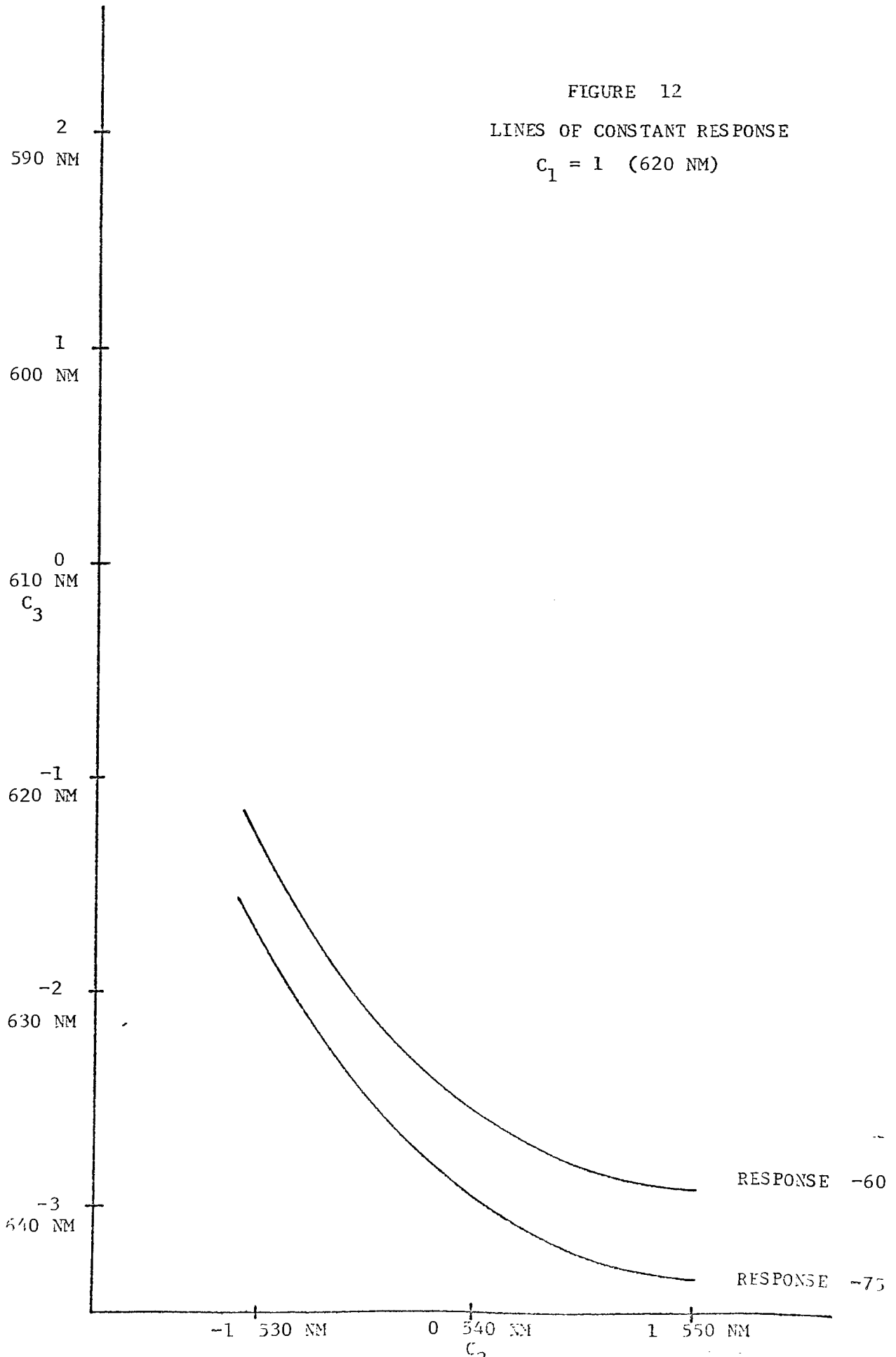


FIGURE 13
 LINES OF CONSTANT RESPONSE
 $c_1 = 0$ (610 NM)

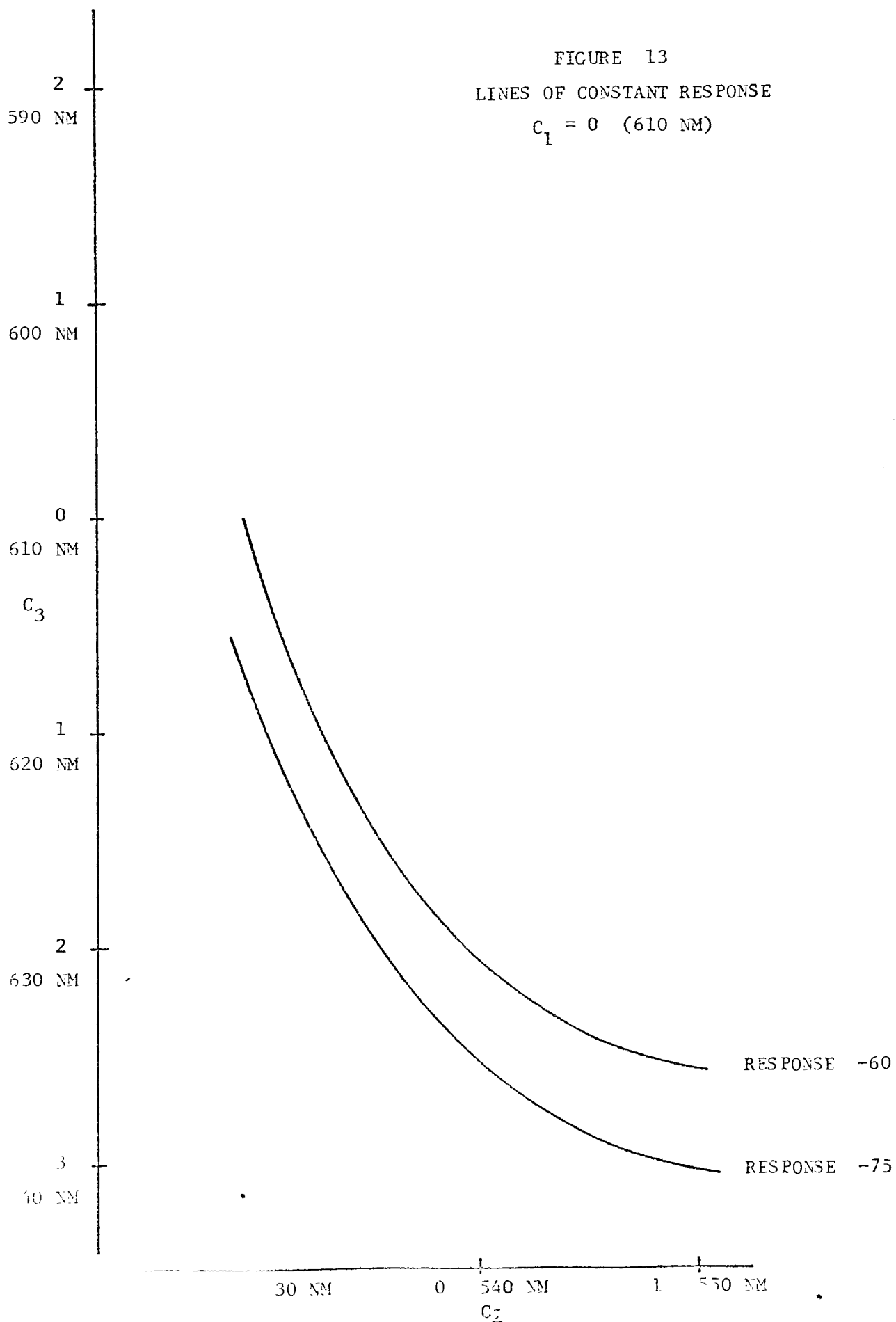
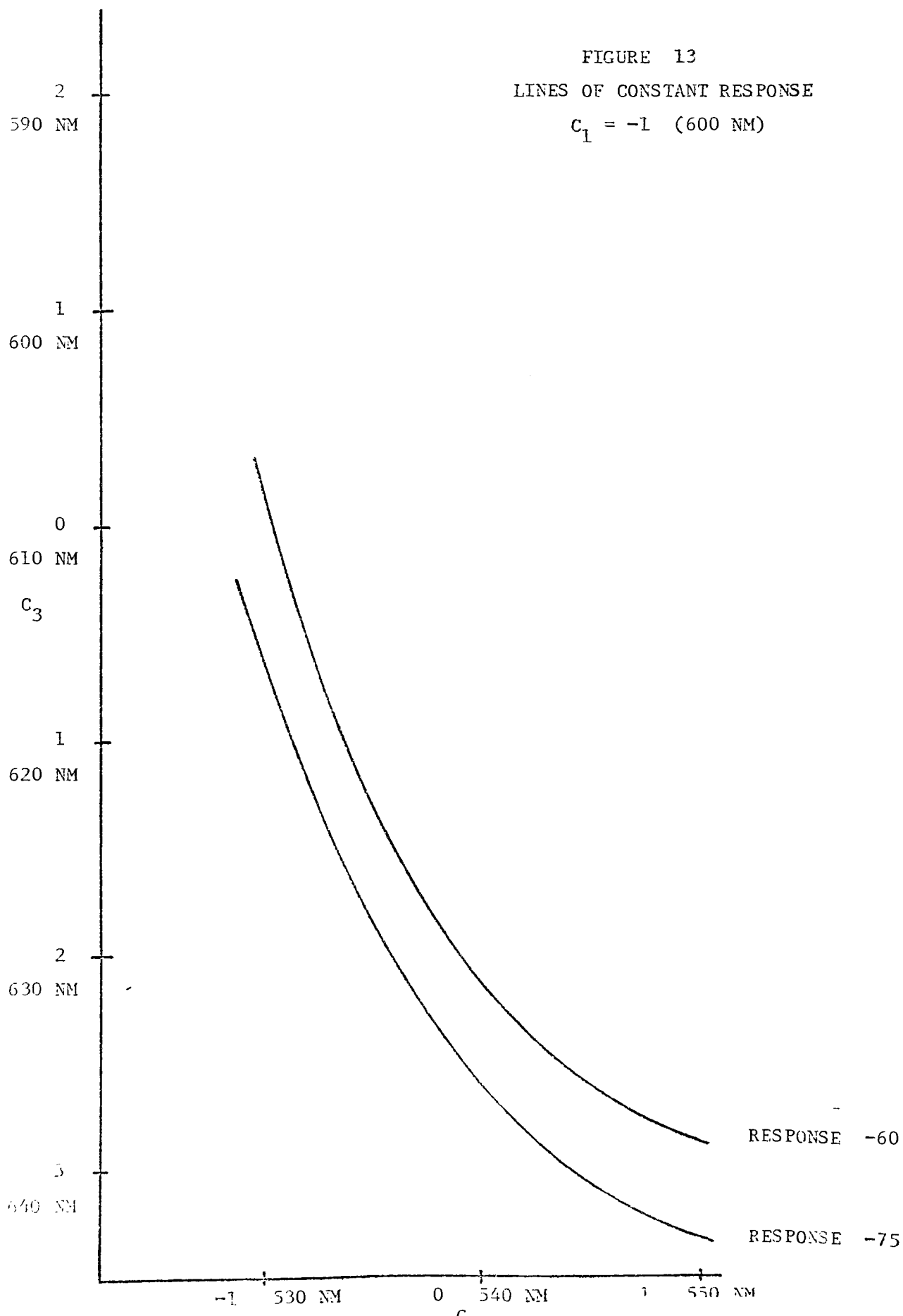


FIGURE 13
 LINES OF CONSTANT RESPONSE
 $c_1 = -1$ (600 NM)



POWER LEVELS FOR THE 3^3 FACTORIAL EXPERIMENT

TREATMENT COMBINATION	FACTOR 1	LEVEL	FACTOR 2	LEVEL	FACTOR 3	LEVEL
-1,-1,-1	600	59.72	530	70.54	440	65.94
-1,-1, 0	600	61.07	530	68.43	450	65.06
-1,-1, 1	600	63.29	530	64.87	460	69.16
-1, 0,-1	600	51.51	540	69.14	440	66.84
-1, 0, 0	600	53.13	540	67.05	450	65.92
-1, 0, 1	600	55.79	540	63.52	460	70.03
-1, 1,-1	600	40.32	550	73.38	440	67.28
-1, 1, 0	600	42.29	550	71.15	450	66.34
-1, 1, 1	600	45.55	550	67.37	460	70.45
0,-1,-1	610	62.08	530	78.02	440	65.77
0,-1, 0	610	63.49	530	76.09	450	64.89
0,-1, 1	610	65.79	530	72.82	460	68.97
0, 0,-1	610	52.78	540	75.38	440	66.78
0, 0, 0	610	54.44	540	73.49	450	65.86
0, 0, 1	610	57.17	540	70.28	460	69.96
0, 1,-1	610	40.52	550	78.46	440	67.27
0, 1, 0	610	42.51	550	75.48	450	66.33
0, 1, 1	610	45.78	550	73.12	460	70.43
1,-1,-1	620	72.04	530	82.41	440	65.67
1,-1, 0	620	73.67	530	80.59	450	64.78
1,-1, 1	620	76.33	530	77.48	460	68.86
1, 0,-1	620	60.74	540	78.96	440	66.75
1, 0, 0	620	62.64	540	77.18	450	65.82
1, 0, 1	620	65.77	540	74.15	460	69.92
1, 1,-1	620	46.12	550	81.29	440	67.26
1, 1, 0	620	48.38	550	79.45	450	66.32
1, 1, 1	620	52.09	550	76.31	460	70.42

COLOR RENDERING INDEX DATA FOR METAMERIC GRAY OBJECTS BASED ON
TREATMENT COMBINATIONS IN THE 3^3 FACTORIAL EXPERIMENT

TREATMENT COMBINATION	CALCULATED CRI	REGRESSION PREDICTED CRI	RESIDUAL
-1,-1,-1	-81.30	-81.99	.69
-1,-1, 0	-65.50	-62.37	-3.13
-1,-1, 1	-56.60	-55.15	-1.45
-1, 0,-1	-34.20	-31.87	-2.33
-1, 0, 0	-17.70	-20.85	3.15
-1, 0, 1	-19.60	-22.24	2.64
-1, 1,-1	-21.80	-22.89	1.09
-1, 1, 0	-20.30	-20.47	.17
-1, 1, 1	-31.30	-30.47	-.83
0,-1,-1	-73.20	-77.09	3.89
0,-1, 0	-56.90	-56.94	.04
0,-1, 1	-47.30	-49.19	1.89
0, 0,-1	-37.00	-34.17	-2.83
0, 0, 0	-22.90	-22.96	.06
0, 0, 1	-24.40	-24.16	-.24
0, 1,-1	-31.90	-32.39	.49
0, 1, 0	-31.50	-30.13	-1.37
0, 1, 1	-42.20	-40.27	-1.93
1,-1,-1	-52.40	-52.07	-.33
1,-1, 0	-32.60	-31.38	-1.22
1,-1, 1	-23.50	-23.11	-.39
1, 0,-1	-17.60	-16.35	-1.25
1, 0, 0	-3.70	-4.95	1.25
1, 0, 1	-6.40	-5.96	-.44
1, 1,-1	-21.20	-21.78	.58
1, 1, 0	-18.60	-19.66	1.06
1, 1, 1	-29.20	-29.94	.74

of CRI exists for a three line spectra and metameric gray object functions it is not within the bounds of this experiment and in any case it is not at the point of maximization when using the standard CIE/CRI reflectance functions. If the point of maximization were the same the lines of constant response would have a point at which the first derivative would be zero which would be inside the boundaries of the experiment and clearly this is not the case.

BIBLIOGRAPHY

1. CIE, "Method of Measuring and Specifying Colour Rendering Properties of Light Sources", CIE Publication 13.2 (1974).
2. Thornton, W. A., "Luminosity and Color-Rendering Capability of White Light", Journal of the Optical Society of America (JOSA), Vol. 61, No. 9, (September 1971), pp. 1155 - 1163.
3. Haft, H. H. and Thornton, W. A., "High Performance Fluorescent Lamps", Journal of IES, (October 1972), pp. 29 - 35.
4. Nayatani, Kurioha, and Sobagaki, "Adequateness of Using 8 Object Colors in Appraising the Color-Matching Properties of Lamps", Journal of Illumination Engineering Institute of Japan, Vol. 54, (1970), pp.461.
5. Ohta, N. and Wyszecki, G., "Theoretical Chromaticity-Mismatch Limits of Metamers Viewed Under Different Illuminants", JOSA, Vol. 65, No. 3, (March 1975), pp. 327 - 333.
6. Wyszecki, and Stiles, Color Science, Wiley (1967), pp. 344
7. Nayatani and Takahama, "Adequateness of Using 12 Metameric Object Colors in Appraising the Color Matching Properties of Lamps", JOSA, Vol. 62, No. 1, (January 1972), pp. 140- 143.
8. Nie, Hull, Jenkins, Steinbrenner, and Bent, Statistical Package for the Social Sciences, McGraw Hill (1970), Second Edition.

APPENDIX A

PRINCIPLE COMPONENT ANALYSIS

In photographic science one is often involved in analysis of multivariate response data which could include such things as families of D Log E curves, modulation transfer functions, reflectances etc. As the amount of data collected increases, the ease of comparison and manipulation decreases; thus it is often desirable to reduce the data to a more manageable result. One method ideally suited for such work is characteristic vector analysis sometimes called principle component analysis. The Application of Characteristic Vector Analysis to Photographic and Optical Response Data by J. L. Simonds in the Journal of the Optical Society of America; August 1963; outlines an algorithm for this type of analysis. The computer program is based on this algorithm. A detailed description is provided in Simonds's article; however a short numerical example is helpful in understanding program operations.

Define a matrix of 3 cases (rows) by 6 variables (columns) as:

$$E_S = \begin{bmatrix} E_1 \\ E_2 \\ E_3 \end{bmatrix} = \begin{bmatrix} 1 & 9 & 8 & 3 & 2 & 4 \\ 3 & 7 & 5 & 8 & 4 & 1 \\ 2 & 5 & 8 & 7 & 3 & 1 \end{bmatrix}$$

The variable (column) average is :

$$\bar{E} = \begin{bmatrix} 2 & 7 & 7 & 6 & 3 & 2 \end{bmatrix}$$

Subtracting \bar{E} from E_s :

$$P = E_s - \bar{E} = \begin{bmatrix} -1 & 2 & 1 & -3 & -1 & 2 \\ 1 & 0 & -2 & 2 & 1 & -1 \\ 0 & -2 & 1 & 1 & 0 & -1 \end{bmatrix}$$

Calculating the variance-covariance matrix:

$$S = P P' = \begin{bmatrix} 2 & -2 & -3 & 5 & 2 & -3 \\ -2 & 8 & 0 & 0 & -2 & 6 \\ -3 & 0 & 6 & -6 & -3 & 3 \\ 5 & -8 & -6 & 14 & 5 & -9 \\ 2 & -2 & -3 & 5 & 2 & -3 \\ -3 & 6 & 3 & -9 & -3 & 6 \end{bmatrix}$$

The trace of S:

$$\text{tr } S = \sum_{i=1}^6 S_{i,i} = 38$$

Arbitrarily defining the first estimate of the characteristic vector:

$$y_0 = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

Calculating the first iteration x_1 :

$$x_1 = S \times y_0 = \begin{bmatrix} 1 & 2 & -3 & 1 & 1 & 0 \end{bmatrix}$$

$$x_1(\text{max}) = 2$$

Normalizing x_1 :

$$y_1 = \frac{x_1}{x_1(\text{max})} = \begin{bmatrix} .5 & 1 & -1.5 & .5 & .5 & 0 \end{bmatrix}$$

Continuing the iteration:

$$x_{11} = \begin{bmatrix} 10.7625 & -18.0152 & -12.5173 & 30.5325 & 10.7625 & -19.7701 \end{bmatrix}$$

$$y_{11} = \begin{bmatrix} .3525 & -.5900 & -.4100 & 1.0000 & .3525 & -.6475 \end{bmatrix}$$

$$x_{12} = \begin{bmatrix} 10.7625 & -18.0152 & -12.5173 & 30.5325 & 10.7625 & -19.7701 \end{bmatrix}$$

At this point x_{11} and x_{12} are equal and the first root is:

$$\lambda_1 = 30.5325$$

The percentage of trace accounted for by the first root is:

$$R = \frac{\lambda_1}{\text{tr } S} \times 100. = \frac{30.5325}{38} \times 100. = 80.35 \%$$

Setting the sum of squares of the elements of x_{12} equal to λ_1 the first characteristic vector is obtained:

$$V^1 = \begin{bmatrix} 1.3180 & -2.2061 & -1.5329 & 3.7390 & 1.3180 & -2.4210 \end{bmatrix}$$

The variance described by the first characteristic vector V^1 is removed from the variance-covariance matrix:

$$S_2 = S - V^1 V^{1'}$$

In determining the second characteristic vector V^2 the variance-covariance matrix S_2 is used and after three iterations:

$$x_3 = \begin{bmatrix} 2.1634 & 7.4674 & -8.0605 & .5931 & 2.1634 & 1.5703 \end{bmatrix}$$

$$\lambda_2 = 7.4674$$

The total trace percentage is:

$$R = \frac{\lambda_1 + \lambda_2}{\text{tr } S} \times 100. = 99.9999 \%$$

Calculating the second characteristic vector V^2 as before:

$$V^2 = \begin{bmatrix} .5128 & 1.7700 & -1.9106 & .1406 & .5128 & .3722 \end{bmatrix}$$

The weighting functions W are determined by:

$$W^i = \frac{V^i}{\lambda_i}$$

for the example

$$W^1 = \begin{bmatrix} .0432 & -.0723 & -.0502 & .1225 & .4317 & -.0793 \end{bmatrix}$$

$$W^2 = \begin{bmatrix} .0687 & .2370 & -.2558 & .0188 & .0687 & .4984 \end{bmatrix}$$

The scalar multipliers are calculated from the original data:

$$Y_1 = \sum_{i=1}^r W_{1,i}(P_{n,i}) \qquad Y_2 = \sum_{i=1}^r W_{2,i}(P_{n,i})$$

where n is the row or case for which the scalars are desired and

r is the number of variables in each set of data or function.

Thus to reconstruct case 2 of the original data the scalars are:

$$Y_1 = .5109 \qquad Y_2 = .6369$$

$$\text{therefore } E_x = \sum_{i=1}^{nv} (V^i \times Y_i) + \bar{E}$$

where nv is the number of characteristic vectors, thus

$$E_2 = \begin{bmatrix} 3 & 7 & 5 & 8 & 4 & 1 \end{bmatrix}$$

In this simple data set the resulting reconstruction is equal to the input function since we have accounted for all the variance. In this simple case principle component analysis is of little value; however its use can be appreciated if in the analysis of a 100 square matrix it would be possible to reduce that data to perhaps three vectors and a set of scalar multipliers.

Program useage

The following description provides an outline of both the job control and data cards required to run program COMPONAL2 on the RIT computer system.

1. JOB statement

```
!JOB acct#,acctname(UCC),7.
```

2. LIMIT statement

```
!LIMIT (CORE,32),(TIME,4),(UO,50),(RERUN)
```

TIME and UO will vary depending on the amount of data.

3. ASSIGN statement

This program provides the capability to write the input data mean, characteristic vectors and reconstructed functions to a permanent disc file with the format 10F10.4. If this option is selected by any of the problems in the job stream the following cards must be provided; otherwise they are not required.

```
!ASSIGN F:1,(FILE,filename1),(OUT),(SAVE)
```

```
!ASSIGN F:2,(FILE,filename2),(OUT),(SAVE)
```

Upon termination of the job filename1 will contain, sequentially, the average of columns, and the characteristic vectors 1 - n. Similarly filename2 will contain the reconstructions of the input functions.

NOTE: Should the job contain more than one problem which selected the write file option the data would be placed in the files in the order in which the problems were run in the job stream.

4. RUN statement

```
!RUN (LMN,COMPANAL2,acct#)
```

where acct# is optional and required only if the program is not in the account in which the job is running.

5. Data Input

A. PROBLM card

Column	Data
1-6	PROBLM
7-9	Number of variables per function ($2 \leq NV \leq 100$)
10-12	Number of cases ($3 \leq NC \leq 50$)
13-15	YES if file write option is desired; otherwise blank.

- 16-18 YES if printing of reconstructions are desired;
 otherwise blank.
- 19-21 Number of variables to be labeled, if desired
 LABELS cards must be provided. ($\leq NV$)
- 22,23 Number of variable format cards <10
- 24-30 Fraction of trace to be accounted for, F7.5 format
 ($.01 \leq PCTN \leq 1.00$) if blank default is for .99 or 99 %.

B. TITLE card

Column	Data
1-5	TITLE
6	blank
7-78	problem title

C. LABELS card (if required)

Column	Data
1-6	LABELS
7-...	Format 7(I4,A6) each variable to be labeled must have its number and associated title punched into a LABELS card. If more than 7 variables are to be labeled then repeat this step until completed.

D. Variable format card

The format card will vary depending on the number of variables in each function and how they are punched into the data cards.

As example if the number of variables were 95 (NV) and each card was punched with 20 values punched in 20F4.3 format the card would be:

(20F4.3/20F4.3/20F4.3/20F4.3/15F4.3)

The '/' being required to skip to the next card resulting in a total of 95 values being read.

E. Data

Punched according to the variable format card specified in D.

Each case must be on a separate set of cards.

(Repeat A - E as required for each problem in the job stream.)

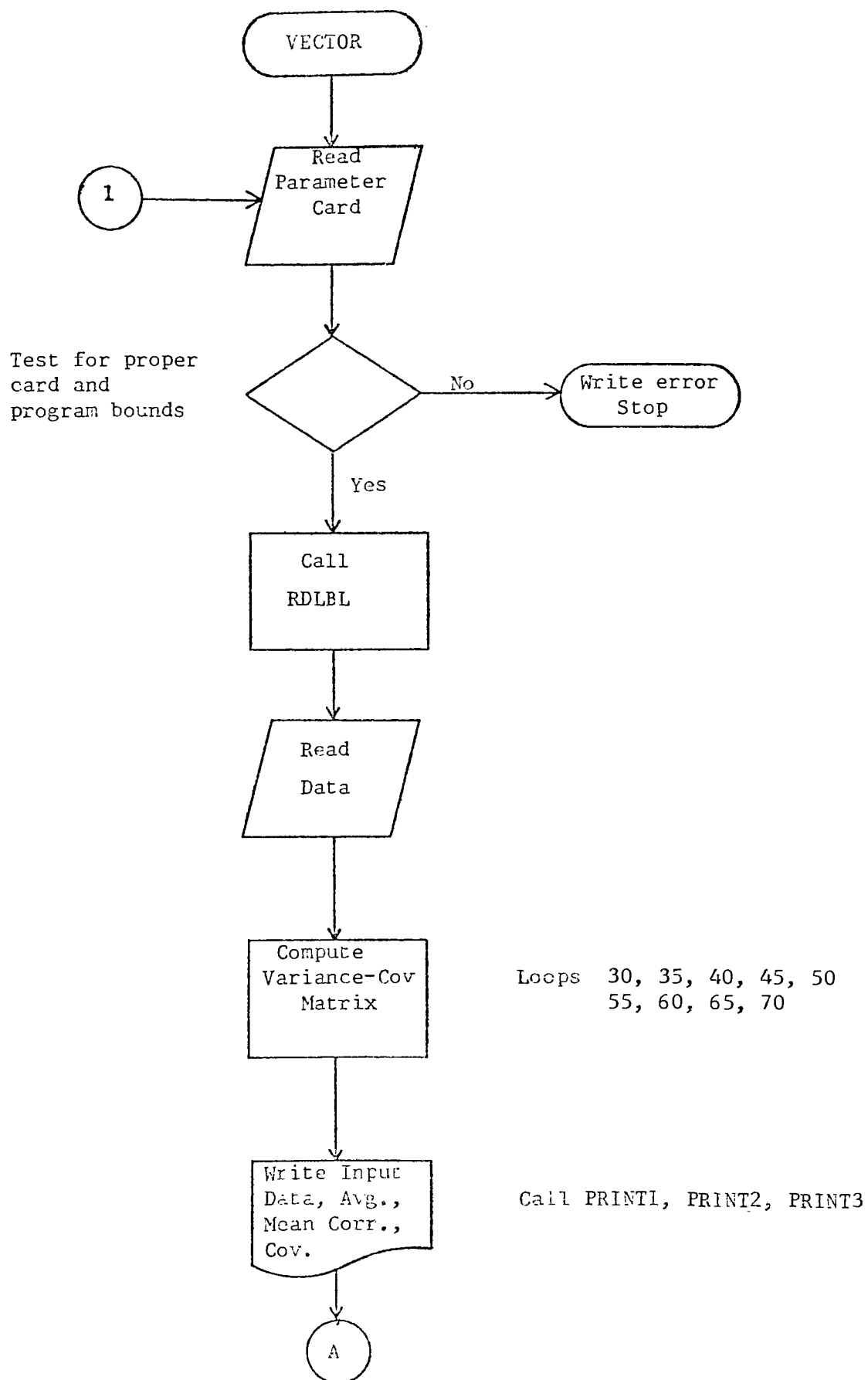
F. FINISH card

Column	Data
--------	------

1-6	FINISH
-----	--------

6. EOD card

!EOD



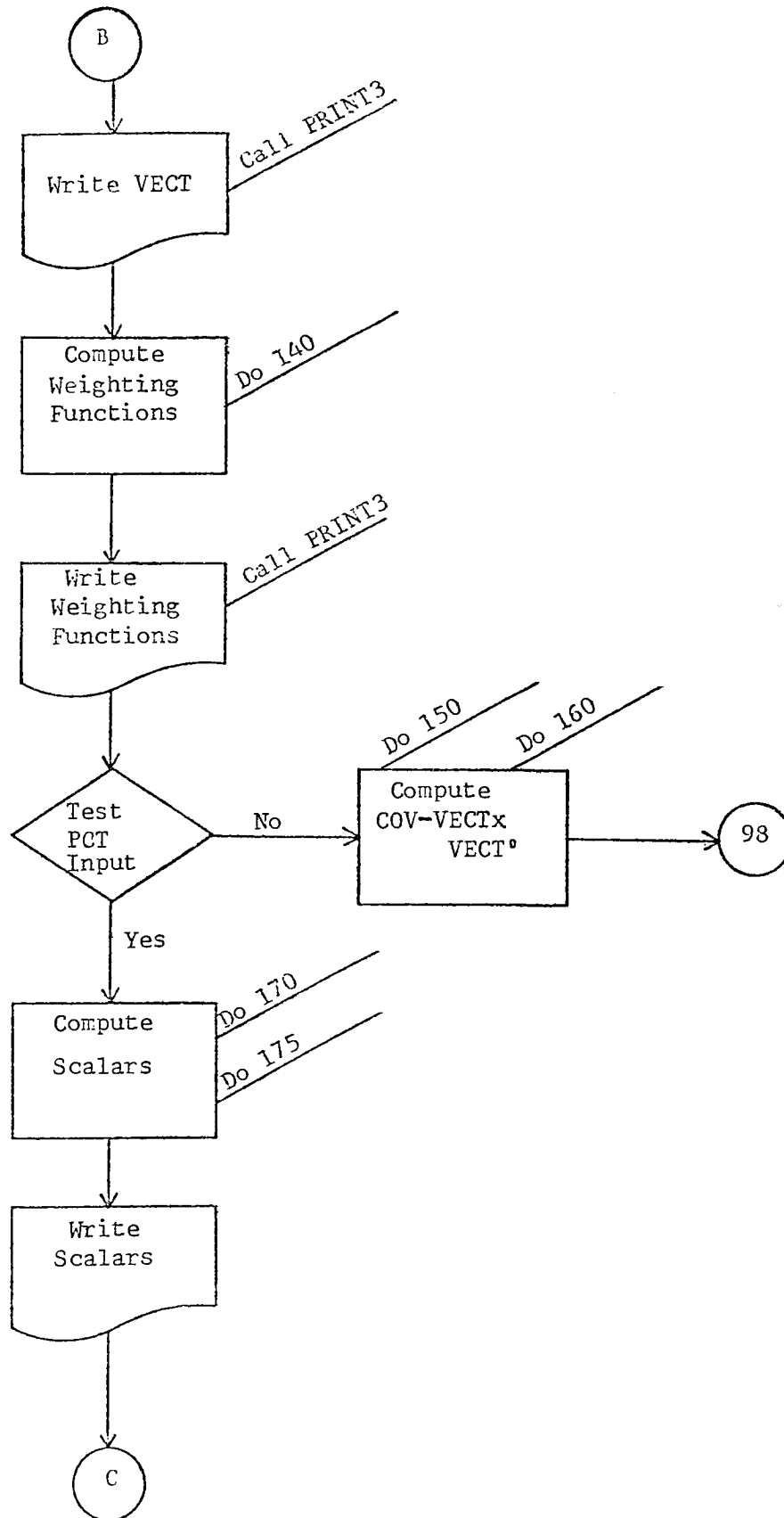


FIGURE A-1 (CONTINUED)

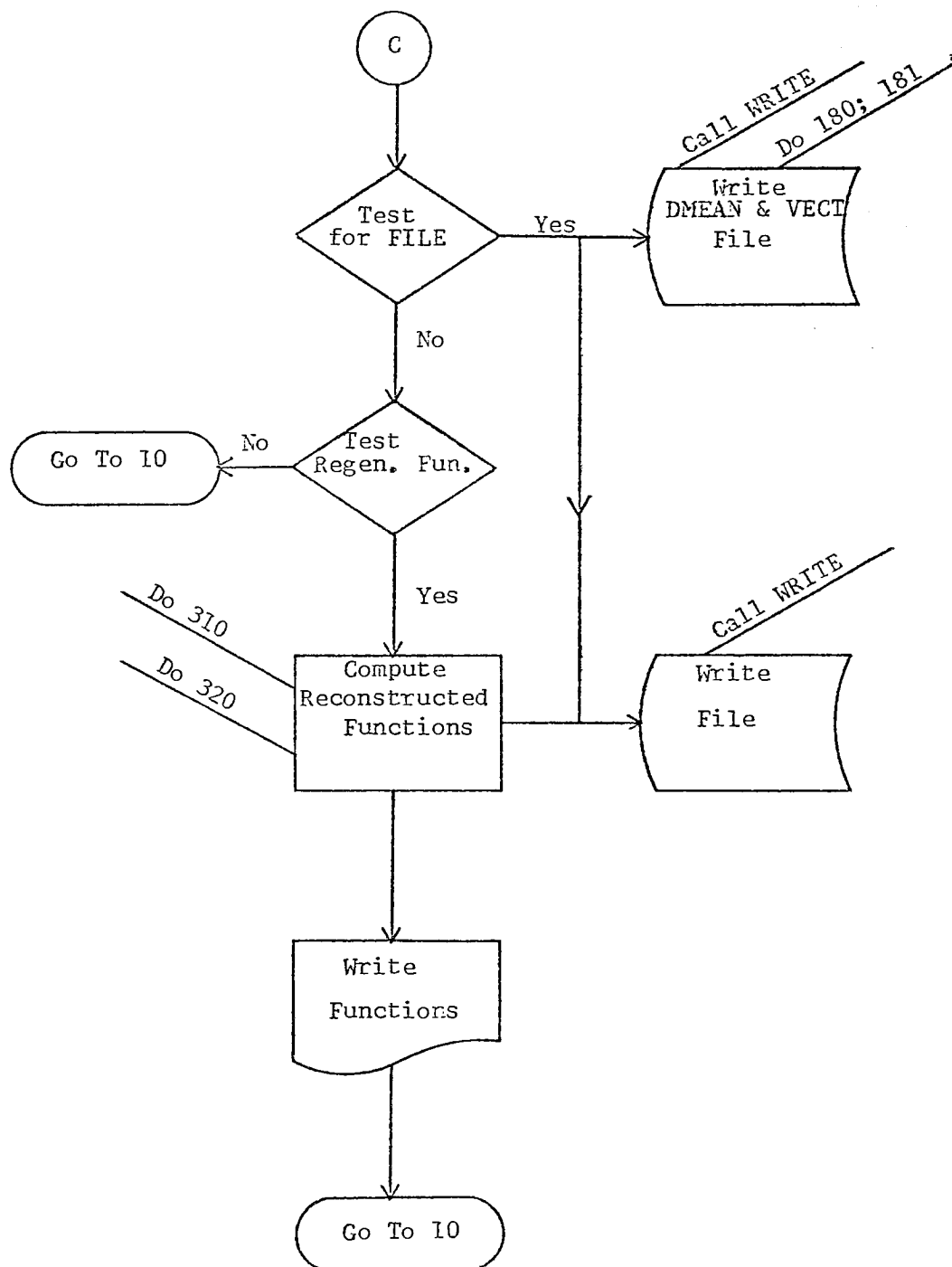


FIGURE A-1 (CONTINUED)

SUBROUTINE WRITE

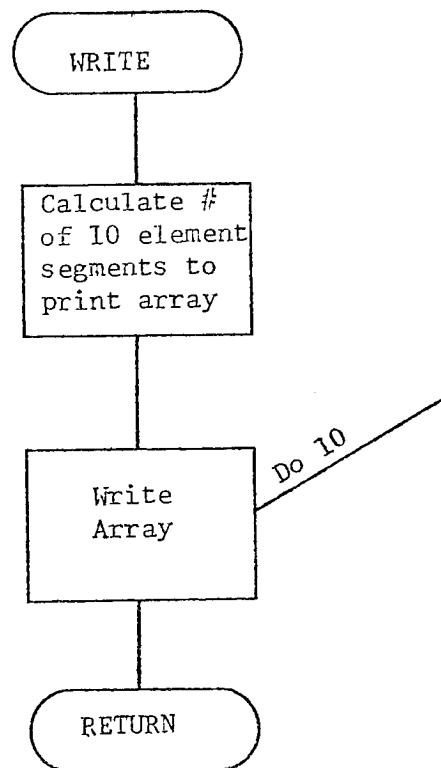


FIGURE A-1 (CONTINUED)

SUBROUTINE RDLBL

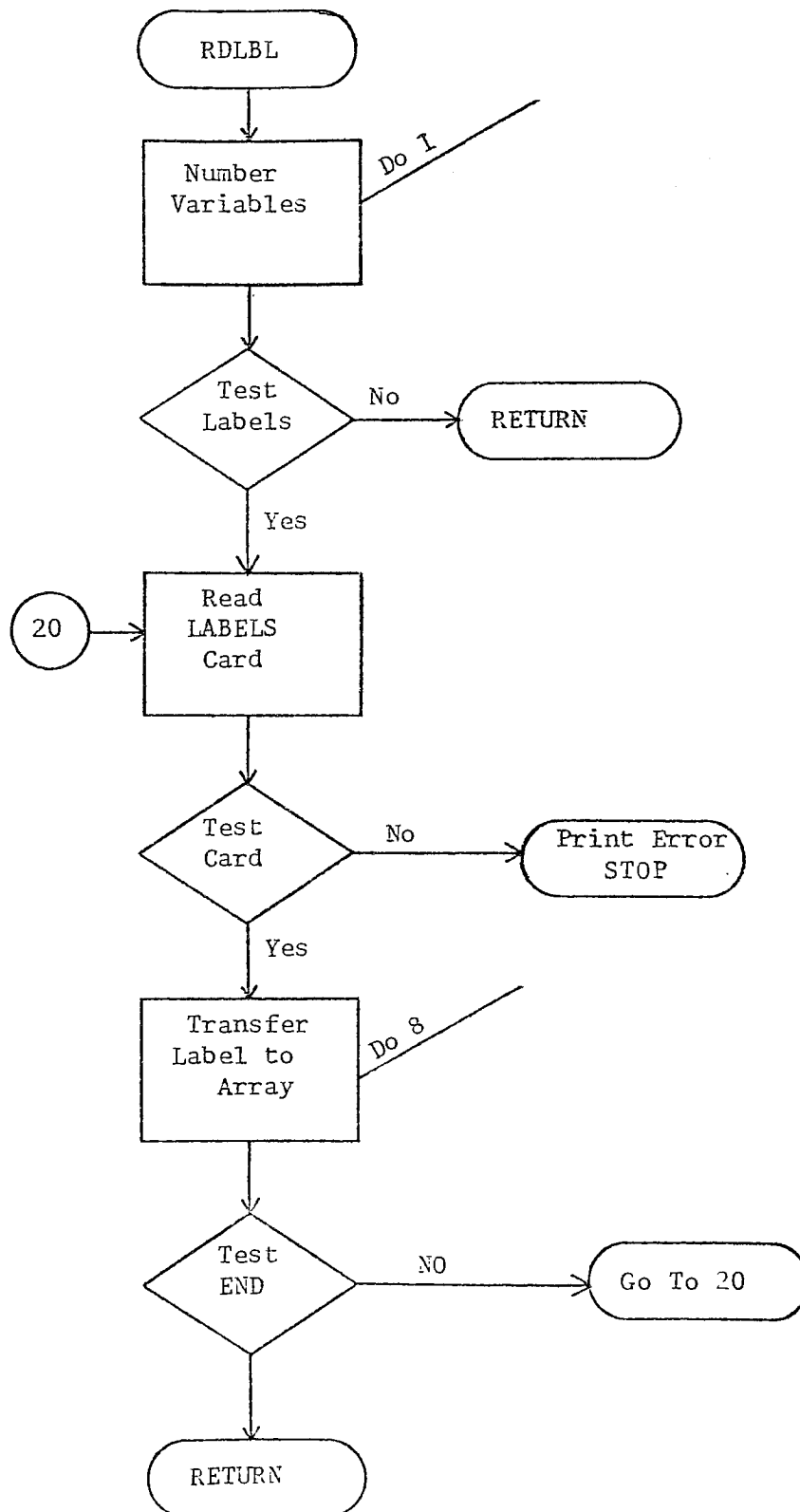


FIGURE A-1 (CONTINUED)

SUBROUTINE PRINT1

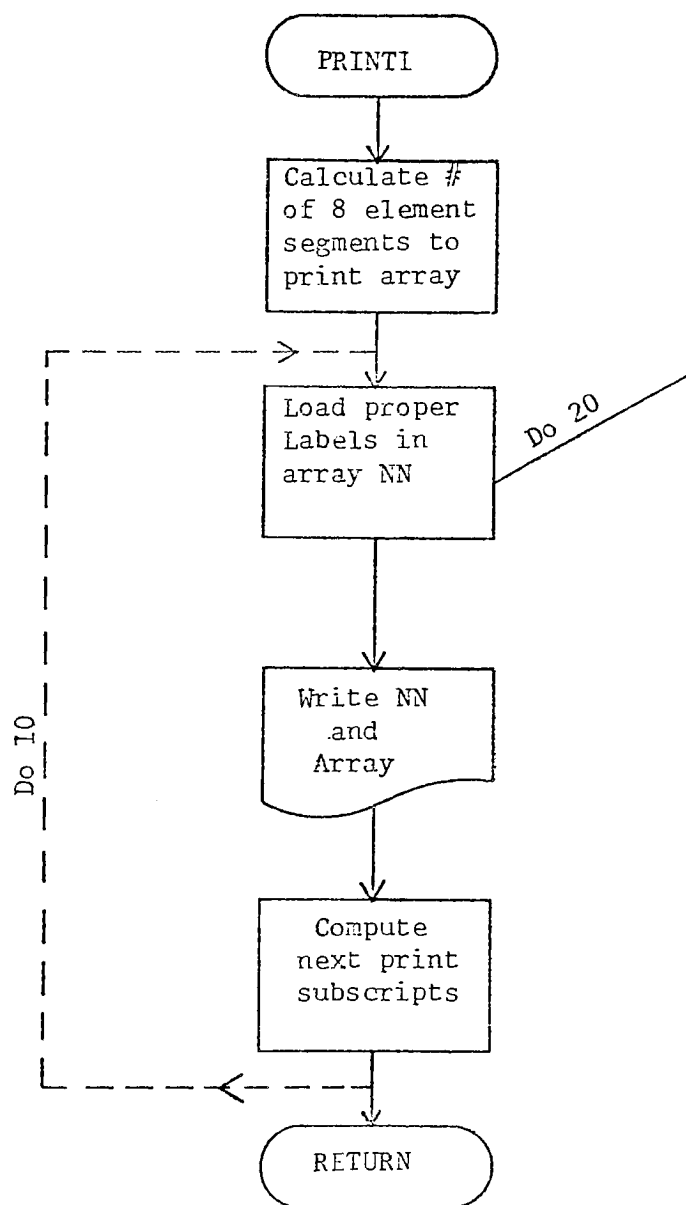


FIGURE A-1 (CONTINUED)

SUBROUTINE PRINT2

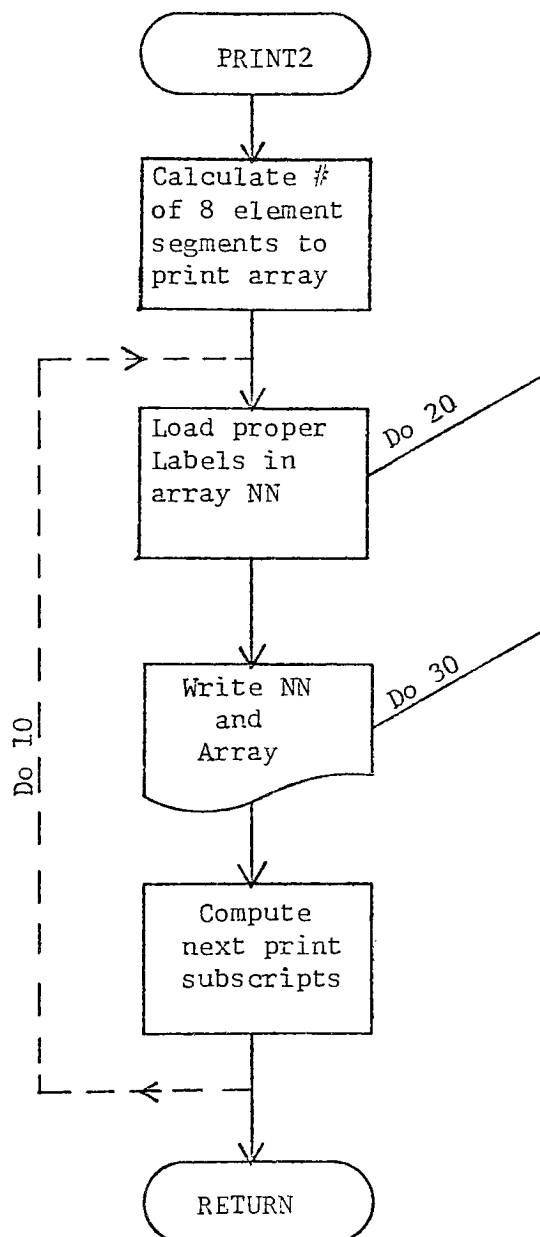


FIGURE A-1 (CONTINUED)

SUBROUTINE PRINT3

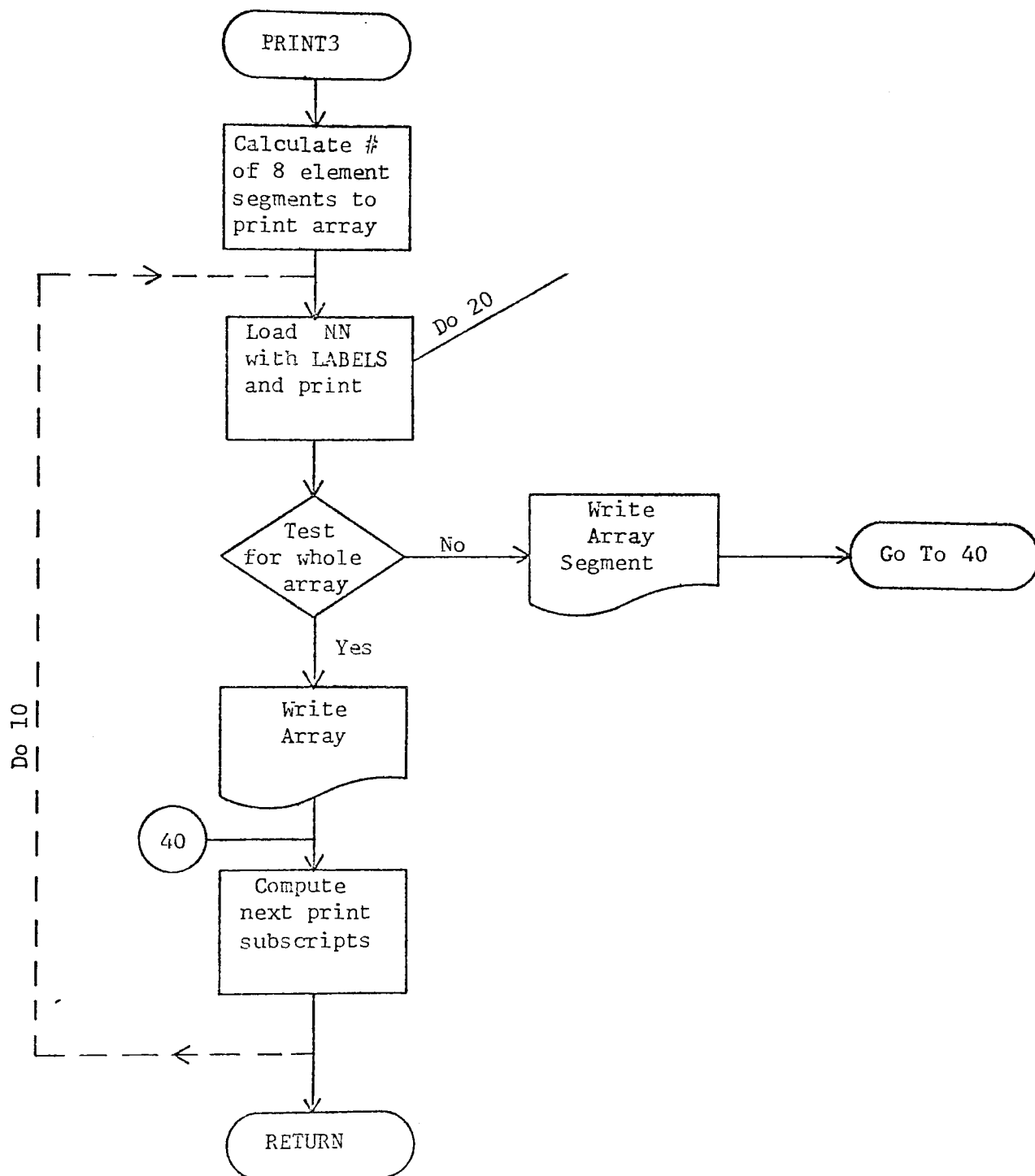


FIGURE A-1 (CONTINUED)

PRINCIPLE COMPONENT ANALYSIS

COMPUTER PROGRAM

FIGURE A-2

PRINCIPLE COMPONENT ANALYSIS FOR BACKGROUND SEE

'APPLICATION OF CHARACTERISTIC VECTOR ANALYSIS TO PHOTOGRAPHIC
AND OPTICAL RESPONSE DATA' J. L. SIMONDS, JOURNAL OF THE
OPTICAL SOCIETY OF AMERICA, VOL. 53, AUGUST 1953, P. 968-974

U IS MATRIX FOR INPUT DATA
DMEAN IS ARRAY OF COLUMN AVERAGES OF MATRIX D
COV IS ARRAY FOR VARIANCE-COVARIANCE MATRIX
VECT IS ARRAY FOR CHARACTERISTIC VECTORS
FMT IS ARRAY FOR VARIABLE FORMAT CARDS
LABELS IS ARRAY OF LABELS FOR INPUT DATA
SCALAR IS ARRAY FOR SCALAR MULTIPLES
TITLE IS ARRAY FOR PROBLEM SET TITLE
U IS COMPUTATIONAL ARRAY
W IS ARRAY OF WEIGHTING FUNCTIONS

DUE TO SIZE RESTRICTIONS, THIS PROGRAM IN IT'S PRESENT VERSION
CAN CALCULATE ONLY 50 CHARACTERISTIC VECTORS BASED ON THE
INPUT DATA. IN ORDER TO INCREASE THE PROGRAM CAPABILITY
THE DIMENSIONS OF VECT, SCALAR, AND W WOULD HAVE TO BE
INCREASED TO 100. THE APPROPRIATE CHANGES IN SUBROUTINES
PRINT2 AND PRINT3 WOULD HAVE TO BE MADE ALSO.

COMMON /ID/LRD,LPU,LPR
REAL*8 A1,B1,C1,D1,E1,F1,G1,H1,I1,J1,K1,L1,M1,N1,O1,P1,Q1,R1,S1,T1,U1,V1,W1,X1,Y1,Z1
DATA A1,B1,C1,D1,E1,F1,G1,H1,I1,J1,K1,L1,M1,N1,O1,P1,Q1,R1,S1,T1,U1,V1,W1,X1,Y1,Z1 /
DIMENSION D(50,100),DMEAN(100),COV(100,100),VECT(50,100),FMT(120),
1 LABELS(100),SCALAR(50,50),TITLE(12),U(100),W(50,100)

COMMON D,COV,VECT,SCALAR,W

10 DEVICE ASSIGNMENTS

LRC=105

LPU=105

LPR=105

10 READ (LRC,900) CODE,NV,NC,PALL,PALL1,LBLV,FCD,PCTN

IF (A1.EQ. CODE) GO TO 15

GO TO 20

12 WRITE (LPR,901) CODE

15 WRITE (LPR,902)

STOP

20 IF (B1.EQ. CODE) GO TO 12

IF (PALL.EQ. 01) PALL=1

IF (PALL1.EQ. 01) PALL1=1

IF (PCTN) 3,5,7

3 PCTN=97

7 READ (LRC,903) CODE, (TITLE(I),I=1,12)

IF (C1.EQ. CODE) GO TO 12

TEST FOR PROBLEM BOUNDS

IF (PALL.EQ. 01) PALL=01

IF ((PCTN-01)*(PCTN-1.001)) 19,202,202

19 IF ((NV-1)*(NV-101)) 21,200,200

21 IF ((NC-2)*(NC-31)) 22,201,201

22 IF (FCD.GT. 0 .AND. FCD.LE. 10) GO TO 24

FCD=1

WRITE (LPR,904)

24 WRITE (LPR,905) (TITLE(I),I=1,12),NV,NC,FCD,PALL,PALL1,PCTN*100.0

CALL ROLBL(LBLV,NV,LABELS)

FCD=FCD*12

READ (LRC,906) (FMT(I),I=1,FCD)

WRITE (LPR,907) (FMT(I),I=1,FCD)

DO 25 I=1,NV

25 READ (LRC,FMT) (D(I,J),J=1,NC)

WRITE (LPR,908)

TESTA=0.0

CALL PRINT3(D,NV,NC,LABELS,0)

FIND AVERAGE D

DO 30 J=1,100

30 DMEAN(J)=0.0

DO 35 I=1,NV

DO 40 J=1,NC

40 DMEAN(J)=DMEAN(J)+D(I,J)/NC

DMEAN(J)=DMEAN(J)/NV

35 CONTINUE

WRITE (LPR,909)

CALL PRINT1(DMEAN,NV,LABELS)

DO 45 I=1,NC

45 IF=1.00


```

50 D(I,J)=U(I,J)-DMEAN(J)
45 CONTINUE
C WRITE MEAN CORRECTED 'D' MATRIX
WRITE (LPR,914)
CALL PRINT3(D,NV,NC,LABELS,0)
C CALCULATE D-TRANSPOSE*D AND ITS TRACE
TRACE=0.0
DO 55 J=1,NV
DO 60 I=1,NV
COV(I,J)=0.0
DO 65 K=1,NC
65 COV(I,J)=COV(I,J)+D(K,J)*D(K,I)
IF (I=J) 60,70,60
70 TRACE=TRACE+COV(I,I)
60 CONTINUE
55 CONTINUE
C WRITE MATRIX AND TRACE
WRITE (LPR,910)
CALL PRINT2(COV,NV,LABELS)
WRITE (LPR,911) TRACE
NVECT=0
93 NVECT=NVECT+1
C TEST FOR >GT. 50 CHARACTERISTIC VECTORS
IF (NVECT >GT. 50) GO TO 302
C SET U ARRAY TO 1
DO 75 I=1,NV
75 U(I)=1.0
C COUNT IS NUMBER OF ITERATIONS/EIGENVALUE
COUNT=0.0
C COMP IS TEST FOR CONVERGENCE
C PRODUCT OF UNIT ROW VECTOR AND COV MATRIX
C CLEAR VECT
96 DO 100 I=1,NV
VECT(NVECT,I)=0.0
C MULTIPLY U BY COV AND STORE IN VECT
DO 100 J=1,NV
100 VECT(NVECT,I)=VECT(NVECT,I)+U(J)*COV(I,J)
COUNT=COUNT+1.0
C FIND MAXIMUM OF VECTOR, SL
105 SL=0.0
DO 110 I=1,NV
IF (VECT(NVECT,I)=SL) 110,110,115
115 SL=VECT(NVECT,I)
110 CONTINUE
C NORMALIZE VECTOR
DO 120 I=1,NV
120 VECT(NVECT,I)=VECT(NVECT,I)/SL
125 COMP=SL*AB
AB=SL
C COMP=TEST IS CONVERGENCE CRITERION
TEST=AB*0.000001
COMP=ABS(COMP)
IF (COMP=TEST) 99,99,121
C DID NOT CONVERGE MOVE VECT(NVECT) TO U
121 DO 125 I=1,NV
125 U(I)=VECT(NVECT,I)
GO TO 96
C CONVERGED, WRITE EIGENVALUE AND NUMBER OF ITERATIONS NEEDED
99 WRITE (LPR,915) NVECT
WRITE (LPR,916) SL
WRITE (LPR,917) COUNT
C TESTA IS SUMMATION OF EIGENVALUES
TESTA=TESTA+SL
C TEST IS PERCENTAGE OF TRACE EXPLAINED BY EIGENVALUES
TEST=TESTA/TRACE
WRITE (LPR,918) TEST
C COMPUTE CHARACTERISTIC VECTOR
SUMS=0.0
DO 130 I=1,NV
130 SUMS=SUMS+VECT(NVECT,I)**2
CUML=SQRT(SL/SUMS)
DO 131 I=1,NV
131 VECT(NVECT,I)=VECT(NVECT,I)*CUML
WRITE (LPR,919)
CALL PRINT3(VECT,NV,NC,LABELS,NVECT)
DO 140 I=1,NV
140 VECT(I)=VECT(NVECT,I)/SL
WRITE (LPR,920)
CALL PRINT3(VECT,NV,NC,LABELS,NVECT)

```

```

IF (PCT=PCTN) 169,169,169
C IF LESS THAN 99 PERCENT, COMPUTE NEXT CHARACTERISTIC VECTOR.
C COMPUTE COV=VECT(NVECT) TRANSPOSE*VECT(NVECT)
159 DO 150 I=1,NV
160 DO 150 J=1,NV
160 COV(I,J)=COV(I,J)+VECT(NVECT,I)*VECT(NVECT,J)
160 CONTINUE
161 GO TO 93
C MORE THAN 99 PERCENT EXPLAINED BY EIGENVALUES
C COMPUTE Y SCALARS
169 WRITE (LPR,952)
DO 170 I=1,NVECT
WRITE (LPR,920) I
DO 170 K=1,NC
SCALAR(I,K)=0.0
DO 175 J=1,NV
175 SCALAR(I,K)=SCALAR(I,K)+W(I,J)*D(K,J)
WRITE (LPR,921) K, SCALAR(I,K)
170 CONTINUE
C PRINT RECONSTRUCTED AND DELTA DATA IF PALL1 .EQ. YES
C CREATE RECONSTRUCTED DATA FROM VECTORS
IF (PALL1 .NE. D1) GO TO 303
PCT=PCT+100.0
WRITE (LPR,954) NVECT,PCT
C WRITE VECTOR FILE IF PALL .EQ. YES
IF (PALL .NE. D1) GO TO 259
CALL WRITE(1,DMEAN,NV,ILOOP)
DO 180 IFLE=1,NVECT
K11=1
K22=MINO(10,NV)
DO 181 JXFL=1,ILOOP
WRITE (1,990) (VECT(IFLE,JFLE),JFLE=K11,K22)
K11=K22+1
K22=MINO(K22,NV)
181 CONTINUE
990 FORMAT (10F10.4)
182 CONTINUE
999 DO 300 I=1,NC
C CLEAR U ARRAY
DO 305 II=1,NV
995 U(II)=0.0
DO 310 J=1,NVECT
DO 320 K=1,NV
420 U(K)=U(K)+SCALAR(J,I)*VECT(J,K)
310 CONTINUE
DO 322 J2=1,NV
322 U(I2)=U(I2)+D*MEAN(I2)
WRITE (LPR,925) I
CALL PRINT(0,NV,LABELS)
C WRITE RECONSTRUCTED FUNCTION FILE IF PALL .EQ. YES
IF (PALL .NE. D1) GO TO 300
CALL WRITE(2,U,NV,ILOOP)
999 CONTINUE
DO 800 I=1,NVECT
WRITE (LPR,980) I
DO 810 J=1,NV
VECTT=VECT(I,J)+D*MEAN(J)
WRITE (LPR,931) LABELS(J),VECT(I,J),D*MEAN(J),VECTT
810 CONTINUE
800 CONTINUE
980 FORMAT (11 VECTOR,11 DATA,11 POINT,11X, VECTOR VALUES)
11X, DATA MEAN,11X, VECTOR + DATA MEAN)
941 FORMAT (2X,A6,1X,5E15.6,14X,E15.6,20X,E15.6)
GO TO 305
999 WRITE (LPR,940)
999 GO TO 10
999 WRITE (LPR,922) NV
999 GO TO 10
999 WRITE (LPR,923) NC
999 GO TO 10
999 WRITE (LPR,960)
PCTA=.99
GO TO 10
999 FORMAT (A6,2I3,2A3,10,1F7.5)
991 FORMAT (1 PROC999 EXPECTED PROBL, TITLE OR FINISH CARD BUT READ
1,96)
999 FORMAT (11 FINISH CARD ENCOUNTERED * PROCESSING ENDED)
999 FORMAT (13A4)
999 FORMAT (11 NUMBER OF VARIABLE FORMAT CARDS INCORRECTLY SPECIFIED, A

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```

905 FORMAT ('1 CHARACTERISTIC VECTOR ANALYSIS - VERSION OF JAN 13, 76',
1//, 'PROBLEM TITLE: ', I12A6, '//', 'NUMBER OF VARIABLES ', I3, '//',
2, 'NUMBER OF CASES ', I3, '//', 'NUMBER OF VARIABLE FORMAT CARDS ',
3I3, '//', 'WRITE VECTOR RECONSTRUCTED FUNCTION FILES: ', I, A3, '//', 'PRI
400 RECONSTRUCTED FUNCTIONS: ', I, A3, '//', 'PERCENT OF TRACE TO BE ACCO
COUNTED FOR ', I, F7.3, '//')
906 FORMAT (18A4)
907 FORMAT ('1 VARIABLE FORMAT IS ', I, '(2X, 18A4), //')
908 FORMAT ('10 INPUT DATA')
909 FORMAT ('10 AVERAGE OF COLUMNS')
910 FORMAT ('11 VARIANCE-COVARIANCE MATRIX')
911 FORMAT ('//', 'TRACE OF VARIANCE-COVARIANCE MATRIX ', E15.6, '////')
914 FORMAT ('11 MEAN CORRECTED MATRIX')
915 FORMAT ('11 VECTOR ', I, F7.3, '10 EIGENVALUE ')
916 FORMAT ('1X, E15.6, '//', '10 NO. OF ITERATIONS')
917 FORMAT (F5.0)
918 FORMAT ('10 SUM EIGENVALUES/TRACE', '//', 1X, E15.6)
919 FORMAT ('10 CHARACTERISTIC VECTOR')
920 FORMAT ('10 CASE ', I5X, '11 SCALAR FOR VECTOR ', I, I3)
921 FORMAT (I7, 18X, E15.6)
922 FORMAT ('1X, I4, ' ORIGINAL VARIABLES IS ILLEGAL')
923 FORMAT ('1X, I4, ' CASES IS ILLEGAL')
924 FORMAT ('10 WEIGHTING FUNCTIONS')
930 FORMAT ('//', 'CASE ', I, '1', '10 RECONSTRUCTED DATA')
940 FORMAT ('11 PROGRAM HAS ATTEMPTED TO CALCULATE MORE THAN 50 CHARACT
11STIC VECTORS', '//', '***** PROCESSING OF THIS PROBLEM DISCONTINUE
20 *****')
952 FORMAT ('11 SCALAR MULTIPLIERS FOR CALCULATED VECTORS')
954 FORMAT('1 ***** VECTOR RECONSTRUCTIONS *****
1-1//', 'RECONSTRUCTIONS ARE BASED ON ', I, I3, ' CHARACTERISTIC VECTORS
2-1//', ' THESE VECTORS ACCOUNT FOR ', I, F7.3, ' % OF THE VARIANCE')
960 FORMAT (2X, I4, '10 PERCENT OF TRACE TO BE ACCOUNTED FOR IS ILLEGAL.
1 SET TO 99 %, '//')
END

```

```
SUBROUTINE WRITE(INO,A,NV,IT)
DIMENSION A(1)
IT=1
XX=10
X1=X2=1
X3=X4=1
X5=X6=1
1 XX=XX+10
IF (NV-XX) 5,5,3
3 IT=IT+1
GO TO 1
5 DO 10 JX=1,IT
WRITE (INO,100) (A(I),I=K1,K2)
X1=X2+1
X3=X4+1
X5=X6+1
10 CONTINUE
100 FORMAT (10F10.4)
RETURN
END
```

SUBROUTINE ROLBL

SUBROUTINE TO READ IN LABELS CARDS, STORE THEM IN ARRAY,
AND SUBSTITUTE NUMBERS FOR UNLABELED VARIABLES

NVAR IS TOTAL NUMBER OF VARIABLES

NLBVAR IS NUMBER OF LABELED VARIABLES EXPECTED

EQUIVALENTS INTEGER AND FLOATING NAMES SO THAT INTEGER SUBTRACTION
MAY BE USED TO TEST ALPHABETIC EQUALITY

REAL*8 ARRAY, ANUMB, DUMY, TEST, ALABEL

DIMENSION ARRAY(1), IDUM(7), DUMY(7)

COMMON /ID/LRD,LPU,LPR

DATA ALABEL/7 LABELS/

NUMBER VARIABLES

DO 1 I=1,NVAR

1 ARRAY(I)=ANUMB(I)

IF NO LABELS, RETURN

IF (NLBVAR) 9,9,2

2 N=0

READ 1 LABELS CARD

20 READ (LRD,3) TEST, (IDUM(J), DUMY(J), J=1,7)

TEST FOR 'LAB' IN FIRST THREE COLS.

IF (TEST=ALABEL) 4,6,4

ERROR PRINT MESSAGE AND QUIT

4 WRITE (LPR,5) TEST

STOP

C EXAMINE 7 FIELDS

6 DO 8 J=1,7

K=IDUM(J)

TEST INDEX, IF 0, IGNORE, IF ILLEGAL, PRINT MESSAGE AND

IGNORE EXCEPT TO COUNT

IF(K) 11,3,10

10 IF (K=NVAR) 7,7,11

11 WRITE (LPR,12) K,DUMY(J)

GO TO 13

C MOVE LABEL TO ARRAY

7 ARRAY(K)=DUMY(J)

C STEP NUMBER OF VARIABLES

13 N=N+1

C TEST FOR END: IF END, RETURN, IF NOT, SCAN OTHER FIELDS:

IF (NLBVAR) 8,9,9

8 CONTINUE

GO TO 20

9 RETURN

10 FORMAT (A6,7(I+,8))

11 FORMAT (' LABELS CARD EXPECTED BUT READ 1, A6)

12 FORMAT (13-CLABELS CARD INDEX,17,13H INCORRECT, LABEL, A6,94 IGNOR

1ED=)

END

FUNCTION ANUMB

THE FUNCTION 'ANUMB' CONVERTS THE INTEGER 111 TO A RIGHT JUSTIFIED ALPHANUMERIC CHARACTERS WHICH ARE RETURNED AS THE HIGH ORDER FOUR BYTES OF THE REAL*8 VARIABLE 'ANUMB'.

REAL*8 GGGG/1 1/2ALPHA

THE ARRAY 'IFAKE' IS A MASK CONSISTING OF THE BINARY CHARACTERS '11110000' MINUS THE BINARY CHARACTERS '01000000'. THE FIRST IS THE MASK WHICH MUST BE ADDED TO AN INTERNAL DIGIT TO MAKE IS ALPHANUMERIC, AND THE SECOND IS THE BINARY CODE FOR A BLANK, WHICH MUST BE SUBTRACTED SINCE 'ALPH' IS INITIALIZED AT BLANKS.

DIMENSION IFAKE(4)

THE FOLLOWING DATA-INITIALIZATION CONSTANTS ARE IN REALITY BINARY MASKS WHICH ARE USED AS THE CRUCIAL KLUDGE WITHIN THIS ROUTINE

THE VALUES ARE, IN ORDER, X'01', X'B0601', X'000000', AND

X'00000000'.

DATA IFAKE/ 176, 45036, 1153+336, -1342177280/

EQUIVALENCE (ALPHA,IALPH)

ALPHA=GGGG

IALPH=

N=0

10 N=N+1

K=MOD(I,10)

SHIFTS 'N=1' BYTES LEFT.

K=K*2*(12*(N-1))

IALPH=IALPH+K+IFAKE(N)

I=I/10

IF (I.NE.0) GO TO 10

ANUMB=ALPHA

RETURN

END

SUBROUTINE PRINT1(NV,LABELS)

56

SUBROUTINE PRINT1 FOR 1 DIMENSIONAL ARRAY

A IS ARRAY TO BE PRINTED

NV IS NUMBER OF VALUES TO BE PRINTED

LABELS IS ARRAY OF LABELS FOR ARRAY A

* NOTE * THIS ROUTINE MUST BE USED WITH SUBROUTINE RDLBL

REAL*8 NN,LABELS

DIMENSION A(1),LABELS(1),NN(8)

COMMON /IO/LPO,LPU,LPR

IT=1

KK=0

K1=1

K2=1+NV

1 KK=KK+8

IF (NV=KK) 5,5,3

3 IT=IT+1

GO TO 1

5 DO 10 JX=1,IT

LLL=K2=K1+1

LL=0

DO 20 JJ=K1,K2

LL=LL+1

20 NN(LL)=LABELS(JJ)

WRITE (LPR,100) (NN(I),I=1,LLL)

WRITE (LPR,101) (A(I),I=K1,K2)

K1=K2+1

K2=K1+7

K2=1+NV

10 CONTINUE

100 FORMAT (///,13X,46,7(3X,46))

101 FORMAT (1H0,7X,4E13.6)

RETURN

END

SUBROUTINE PRINT2 FOR PRINTING OF LABELED SYMMETRIC MATRICES

A IS ARRAY TO BE PRINTED

N IS NUMBER OF VALUES TO BE PRINTED

LABELS IS ARRAY OF LABELS FOR TITLING OF ARRAY A

* NOTE * THIS ROUTINE MUST BE USED WITH SUBROUTINE RDLBL

REAL*8 N,LABELS

DIMENSION A(100,100), LABELS(1), NN(8)

COMMON /IO/LPD,LPU,LPR

IT=1

KK=0

K1=IT

K2=MINO(8,N)

1 KK=KK+3

IF (N=KK) 5,5,3

3 IT=IT+1

GO TO 1

5 DO 10 JX=1,IT

LLL=K2=K1+1

DO 20

20 JJ=K1,K2

LL=LL+1

20 N(LL)=LABELS(JJ)

WRITE (LPR,100) (N(I),I=1,LLL)

WRITE (LPR,102)

DO 30 I=1,N

30 WRITE (LPR,101) LABELS(I), (A(I,J),J=K1,K2)

K1=K2+1

K2=K1+7

K2=MINO(K2,N)

10 CONTINUE

100 FORMAT (1//,13X,A6,7(9X,A6))

101 FORMAT (1H ,A6,1X,8E15.5)

102 FORMAT (1H)

RETURN

END

SUBROUTINE PRINT3(A,NC,NR,LABELS,JK)

58

SUBROUTINE PRINT3 FOR PRINTING LABELED ARRAYS

A IS ARRAY TO BE PRINTED

NC IS NUMBER OF COLUMNS

NR IS NUMBER OF ROWS

LABELS IS ARRAY OF LABELS FOR TITLING OF ARRAY A

* NOTE * THIS ROUTINE MUST BE USED WITH SUBROUTINE RDLBL

JK IS INDICATOR

0 - PRINTS ENTIRE ARRAY

N - PRINTS THE N(TH) ROW OF ARRAY A

REAL*8 NN,LABELS

DIMENSION A(50,100), LABELS(1), NN(2)

COMMON /IO/LRD,LPU,LPR

IT=1

KK=0

K1=IT

K2=MIN0(8,NC)

1 KK=KK+8

IF (NC=KK) 5,5,3

3 IT=IT+1

GO TO 1

5 DO 10 JK=1,IT

LLL=K2=K1+1

LL=0

DO 20 JJ=K1,K2

LL=LL+1

20 NN(LL)=LABELS(JJ)

WRITE (LPR,100) (NN(IT),IT=1,LLL)

WRITE (LPR,102)

IF (JK=NR) GO TO 35

DO 30 I=1,NR

30 WRITE (LPR,101) I,(A(I,J),J=K1,K2)

GO TO 40

35 WRITE (LPR,101) JK,(A(JK,J),J=K1,K2)

40 K1=K2+1

K2=K1+7

K2=MIN0(K2,NC)

10 CONTINUE

100 FORMAT (///,13X,A6,7(9X,A6))

101 FORMAT (1H,15,1X,8E15.5)

102 FORMAT (1H)

RETURN

END

APPENDIX B

REFLECTANCES OF 12 GRAY OBJECT COLORS METAMERIC WITH RESPECT
TO THE 1931 CIE STANDARD OBSERVER AND CIE SOURCE C
(WYSZECKI 1962)

WAVELENGTH (NM)	1	2	3	4	5	6
380	.0575	.0437	.1613	.1148	.0243	.2550
390	.2017	.1081	.1770	.1170	.0414	.2919
400	.3510	.1766	.2173	.1243	.0608	.3150
410	.4419	.2279	.2579	.1257	.0819	.3268
420	.4762	.2590	.2895	.1301	.1014	.3314
430	.4617	.2834	.3064	.1330	.1298	.3327
440	.4197	.2964	.3126	.1342	.1565	.3297
450	.3529	.3004	.3089	.2992	.2858	.3230
460	.2744	.3073	.2961	.4887	.4389	.3121
470	.1617	.3023	.2595	.4770	.4637	.2877
480	.0851	.3073	.2350	.3742	.4341	.2478
490	.0634	.3285	.3426	.2607	.3983	.2012
500	.0637	.3535	.4321	.2874	.3796	.1634
510	.0653	.3708	.4478	.4496	.3649	.1210
520	.0664	.3769	.4269	.4852	.3555	.0654
530	.0677	.3664	.3798	.4136	.3397	.2039
540	.1404	.3354	.3233	.3123	.3098	.4011
550	.5696	.2851	.2707	.2222	.2643	.3582
560	.6792	.2147	.2275	.1676	.2002	.2929
570	.6046	.1465	.1985	.1558	.1362	.3819
580	.4811	.0890	.1812	.1893	.0818	.5962
590	.3513	.2425	.1702	.2394	.2734	.5061
600	.2360	.6854	.1647	.2979	.7078	.3429
610	.1433	.5856	.1705	.3520	.5950	.2065
620	.0809	.3676	.3035	.4021	.3832	.1179
630	.0422	.2145	.7796	.4401	.2282	.0626
640	.0188	.1177	.8000	.4737	.1259	.0291
650	.0094	.0589	.6492	.5029	.0629	.0128
660	.0031	.0294	.4984	.5249	.0315	.0074
670	.0016	.0126	.3924	.5424	.0157	.0083
680	.0000	.0042	.3117	.5578	.0079	.0113
690	.0000	.0000	.2694	.5724	.0039	.0181
700	.0059	.0019	.2530	.5812	.0000	.0223
710	.0188	.0061	.2497	.5885	.0000	.0231
720	.0282	.0092	.2438	.5958	.0000	.0223
730	.0493	.0161	.2394	.6024	.0000	.0210
740	.0634	.0206	.2329	.6089	.0000	.0202
750	.0728	.0237	.2297	.6148	.0000	.0189
760	.0821	.0268	.2305	.6199	.0000	.0181

REFLECTANCES OF 12 GRAY OBJECT COLORS METAMERIC WITH RESPECT
TO THE 1931 CIE STANDARD OBSERVER AND CIE SOURCE C
(WYSZECKI 1962)

WAVELENGTH (NM)	7	8	9	10	11	12
380	.6061	.2190	.2706	.2411	.3749	.1042
390	.6017	.2208	.2945	.3158	.3781	.1101
400	.5503	.2208	.3096	.3703	.3770	.1168
410	.4611	.2225	.3172	.4026	.3715	.1220
420	.3748	.2243	.3202	.4167	.3655	.1299
430	.3230	.2261	.3210	.4106	.3569	.1364
440	.2986	.2296	.3191	.3915	.3451	.1443
450	.2890	.2350	.3148	.3521	.3299	.1563
460	.2847	.2668	.3077	.2906	.3086	.2258
470	.2825	.3985	.2918	.1933	.2711	.5199
480	.2816	.5283	.2685	.0960	.2184	.8121
490	.2812	.4980	.2408	.0494	.1614	.7539
500	.2812	.4023	.2171	.0644	.1197	.5457
510	.2811	.3528	.1954	.2878	.0737	.3787
520	.2830	.2454	.1593	.5860	.0433	.2799
530	.3029	.3171	.1475	.5752	.0553	.2296
540	.3335	.2877	.2315	.4341	.1910	.2141
550	.3254	.2620	.4136	.2822	.4895	.2048
560	.3094	.2433	.5146	.1664	.6621	.2029
570	.2971	.2322	.4711	.0904	.6002	.2165
580	.2895	.2253	.3723	.0472	.4536	.2485
590	.2849	.2222	.2813	.2467	.3176	.2839
600	.2822	.2206	.2143	.6708	.2161	.3208
610	.2810	.2251	.1727	.5661	.1520	.3587
620	.2815	.3164	.1446	.3673	.1164	.3937
630	.2915	.6399	.1326	.2175	.0956	.4207
640	.3394	.6538	.1729	.1200	.0912	.4477
650	.3568	.5513	.4231	.0600	.0871	.4707
660	.2490	.4488	.6223	.0300	.0878	.4888
670	.3385	.3768	.6528	.0150	.0953	.5044
680	.3314	.3215	.6163	.0075	.1310	.5180
690	.3443	.2892	.5720	.0037	.2155	.5298
700	.3938	.2633	.5265	.0000	.3231	.5381
710	.4556	.2467	.4826	.0000	.3886	.5455
720	.5062	.2356	.4422	.0000	.4252	.5532
730	.5481	.2273	.4078	.0000	.4429	.5602
740	.5817	.2218	.3717	.0000	.4474	.5669
750	.5999	.2190	.3436	.0000	.4495	.5730
760	.5859	.2190	.3137	.0000	.4518	.5787

CIE/CI STANDARD REFLECTANCE FUNCTIONS

WAVELENGTH

	1	2	3	4	5	6	7	8
380	.1160	.0530	.0580	.0570	.1430	.0770	.1500	.0750
385	.1360	.0550	.0590	.0590	.1370	.0810	.1770	.0780
390	.1590	.0590	.0610	.0620	.1230	.0890	.2180	.0840
395	.1900	.0640	.0630	.0670	.1270	.1130	.2930	.0900
400	.2190	.0700	.0650	.0740	.1290	.1510	.3790	.1040
405	.2390	.0790	.0690	.0830	.1300	.2030	.4590	.1290
410	.2520	.0890	.0700	.0920	.1310	.2650	.5240	.1700
415	.2560	.1010	.0720	.1050	.1320	.3390	.5460	.2400
420	.2560	.1110	.0730	.1160	.1330	.4100	.5510	.3190
425	.2540	.1160	.0730	.1210	.1350	.4640	.5550	.4160
430	.2520	.1180	.0740	.1240	.1370	.4920	.5590	.4620
435	.2480	.1200	.0740	.1260	.1380	.5060	.5600	.4820
440	.2440	.1210	.0740	.1280	.1390	.5170	.5610	.4900
445	.2400	.1220	.0730	.1310	.1400	.5240	.5600	.4880
450	.2370	.1220	.0730	.1350	.1410	.5310	.5560	.4820
455	.2320	.1220	.0730	.1390	.1420	.5300	.5510	.4730
460	.2300	.1230	.0730	.1440	.1430	.5340	.5440	.4620
465	.2260	.1240	.0730	.1510	.1440	.5310	.5370	.4500
470	.2250	.1270	.0740	.1610	.1460	.5360	.5220	.4390
475	.2220	.1280	.0750	.1720	.1470	.5360	.5060	.4260
480	.2200	.1310	.0760	.1860	.1480	.5340	.4800	.4130
485	.2180	.1340	.0800	.2030	.1490	.5290	.4590	.3970
490	.2160	.1380	.0850	.2290	.1500	.5210	.4400	.3820
495	.2140	.1430	.0940	.2540	.1510	.5100	.4290	.3660
500	.2140	.1500	.1090	.2810	.1520	.5000	.4000	.3520
505	.2140	.1590	.1260	.3080	.1530	.5040	.3850	.3370
510	.2160	.1740	.1480	.3320	.1540	.4880	.3630	.3250
515	.2180	.1900	.1720	.3520	.1550	.4690	.3410	.3100
520	.2230	.2070	.1980	.3700	.1560	.4500	.3240	.2970
525	.2250	.2250	.2210	.3830	.1570	.4310	.3110	.2890
530	.2260	.2420	.2410	.3900	.1580	.4140	.3010	.2830
535	.2260	.2530	.2600	.3940	.1590	.3950	.2910	.2760
540	.2250	.2600	.2780	.3950	.1600	.3770	.2830	.2700
545	.2250	.2640	.3020	.3920	.1610	.3580	.2730	.2620
550	.2270	.2670	.3390	.3850	.1620	.3410	.2650	.2560
555	.2300	.2690	.3700	.3770	.1630	.3250	.2600	.2510
560	.2340	.2720	.3920	.3670	.1640	.3090	.2570	.2500
565	.2450	.2760	.3990	.3540	.1650	.2930	.2570	.2510
570	.2610	.2820	.4000	.3410	.1660	.2790	.2590	.2540
575	.2820	.2890	.3900	.3270	.1670	.2650	.2600	.2580
580	.3120	.2970	.3800	.3130	.1680	.2530	.2600	.2640
585	.3530	.3090	.3650	.2960	.1690	.2410	.2600	.2690
590	.4070	.3200	.3490	.2800	.1700	.2300	.2600	.2720
595	.4800	.3300	.3320	.2620	.1710	.2200	.2600	.2780
600	.5800	.3400	.3150	.2400	.1720	.2100	.2600	.2790
605	.7100	.3500	.2980	.2100	.1730	.2000	.2600	.2790
610	.8700	.3600	.2800	.1800	.1740	.1900	.2600	.2790
615	.9700	.3700	.2600	.1500	.1750	.1800	.2600	.2790
620	1.0000	.3800	.2400	.1200	.1760	.1700	.2600	.2790
625	1.0000	.3900	.2200	.0900	.1770	.1600	.2600	.2790
630	1.0000	.4000	.2000	.0600	.1780	.1500	.2600	.2790
635	1.0000	.4100	.1800	.0300	.1790	.1400	.2600	.2790
640	1.0000	.4200	.1600	.0000	.1800	.1300	.2600	.2790
645	1.0000	.4300	.1400	.0000	.1810	.1200	.2600	.2790
650	1.0000	.4400	.1200	.0000	.1820	.1100	.2600	.2790
655	1.0000	.4500	.1000	.0000	.1830	.1000	.2600	.2790
660	1.0000	.4600	.0800	.0000	.1840	.0900	.2600	.2790
665	1.0000	.4700	.0600	.0000	.1850	.0800	.2600	.2790
670	1.0000	.4800	.0400	.0000	.1860	.0700	.2600	.2790
675	1.0000	.4900	.0200	.0000	.1870	.0600	.2600	.2790
680	1.0000	.5000	.0000	.0000	.1880	.0500	.2600	.2790
685	1.0000	.5100	.0000	.0000	.1890	.0400	.2600	.2790
690	1.0000	.5200	.0000	.0000	.1900	.0300	.2600	.2790
695	1.0000	.5300	.0000	.0000	.1910	.0200	.2600	.2790
700	1.0000	.5400	.0000	.0000	.1920	.0100	.2600	.2790

RECONSTRUCTED CIE/CRI REFLECTANCE FUNCTIONS: 3 COMPONENT

Wavelength

(nm)	1	2	3	4	5	6	7	8
350	.0950	.0805	.0317	.0794	.1150	.1073	.1233	.0976
360	.1098	.0937	.0212	.0935	.1422	.1227	.1437	.1051
370	.1279	.1076	.0105	.1086	.1731	.1458	.1722	.1195
380	.1497	.1192	-.0007	.1203	.2097	.1833	.2171	.1485
390	.1712	.1265	-.0021	.1332	.2458	.2303	.2701	.1870
400	.1892	.1280	-.0070	.1402	.2761	.2827	.3253	.2317
410	.2050	.1259	.0002	.1436	.3004	.3366	.3804	.2809
420	.2185	.1220	.0201	.1465	.3152	.3878	.4302	.3327
430	.2305	.1172	.0421	.1425	.3239	.4337	.4753	.3837
440	.2473	.1128	.0615	.1317	.3237	.4720	.5211	.4440
450	.2547	.1102	.0712	.1279	.3258	.4932	.5445	.4725
460	.2565	.1090	.0759	.1273	.3222	.5050	.5553	.4839
470	.2562	.1064	.0779	.1284	.3313	.5125	.5607	.4875
480	.2535	.1032	.0783	.1318	.3355	.5170	.5612	.4835
490	.2499	.1039	.0791	.1364	.3405	.5217	.5608	.4777
500	.2446	.1030	.0799	.1418	.3459	.5260	.5583	.4695
510	.2403	.1024	.0803	.1491	.3526	.5288	.5547	.4577
520	.2348	.1021	.0818	.1571	.3594	.5319	.5499	.4451
530	.2315	.1054	.0846	.1674	.3671	.5328	.5437	.4317
540	.2269	.1086	.0869	.1793	.3737	.5309	.5342	.4149
550	.2239	.1147	.0902	.1908	.3821	.5279	.5237	.3932
560	.2209	.1226	.0944	.2005	.3918	.5237	.5188	.3733
570	.2187	.1325	.1021	.2230	.3992	.5169	.4954	.3535
580	.2170	.1433	.1130	.2402	.4037	.5096	.4790	.3322
590	.2170	.1568	.1301	.2583	.4116	.5006	.4607	.3126
600	.2176	.1716	.1491	.2776	.4146	.4886	.4398	.2922
610	.2214	.1894	.1725	.2963	.4153	.4749	.4190	.2761
620	.2249	.2070	.1966	.3136	.4131	.4583	.3959	.2596
630	.2311	.2254	.2221	.3292	.4096	.4422	.3756	.2487
640	.2369	.2418	.2439	.3421	.4055	.4268	.3574	.2396
650	.2427	.2532	.2626	.3505	.3993	.4125	.3424	.2348
660	.2459	.2632	.2793	.3560	.3907	.3977	.3267	.2294
670	.2474	.2722	.2944	.3589	.3812	.3848	.3128	.2254
680	.2472	.2777	.3137	.3610	.3684	.3712	.2965	.2212
690	.2466	.2830	.3434	.3634	.3521	.3605	.2807	.2219
700	.2471	.2873	.3677	.3639	.3371	.3505	.2676	.2239
710	.2504	.2919	.3841	.3611	.3226	.3398	.2580	.2292
720	.2544	.2962	.3872	.3539	.3059	.3246	.2524	.2364
730	.2634	.3032	.3854	.3406	.2990	.3112	.2494	.2407
740	.2713	.3083	.3773	.3253	.2890	.2959	.2476	.2528
750	.2813	.3080	.3647	.32	.27	.2786	.2433	.2620
760	.2916	.3070	.3500	.3136	.2711	.2690	.2411	.2702
770	.3020	.3117	.3337	.3023	.2636	.2656	.2437	.2786
780	.3126	.3243	.3200	.2900	.2560	.2600	.2411	.2777
790	.3230	.3400	.3100	.2750	.2480	.2540	.2400	.2810
800	.3340	.3500	.3000	.2600	.2400	.2460	.2300	.2846
810	.3460	.3600	.3000	.2450	.2320	.2380	.2200	.2841
820	.3610	.3600	.2610	.2300	.2240	.2300	.2120	.2840
830	.3710	.3600	.2400	.2150	.2180	.2240	.2060	.2840
840	.3810	.3600	.2400	.2000	.2100	.2160	.2000	.2840

RECONSTRUCTED SIE/CRI REFLECTANCE FUNCTIONS: 3 COMPONENT
(CONTINUED)

WAVELENGTH

	1	2	3	4	5	6	7	8
600	.4084	.3412	.2471	.1911	.2042	.1908	.3439	.4626
610	.4240	.3422	.2485	.1933	.1965	.2032	.3457	.4789
620	.4372	.3419	.2438	.1928	.1902	.2105	.3846	.5319
630	.4474	.3403	.2417	.1910	.1852	.2175	.4051	.5599
640	.4566	.3390	.2402	.1869	.1815	.2247	.4222	.5849
650	.4624	.3341	.2384	.1800	.1791	.2313	.4355	.6033
660	.4675	.3357	.2365	.1829	.1786	.2374	.4468	.6177
670	.4706	.3333	.2351	.1834	.1785	.2442	.4570	.6299
680	.4729	.3310	.2353	.1802	.1790	.2518	.4664	.6405
690	.4747	.3296	.2360	.1835	.1797	.2574	.4731	.6482
700	.4765	.3298	.2391	.1873	.1800	.2633	.4793	.6559
710	.4772	.3271	.2439	.1970	.1809	.2695	.4847	.6616
720	.4789	.3288	.2493	.199	.1812	.2756	.4887	.6669
730	.4799	.3297	.2544	.1984	.1843	.2809	.4918	.6707
740	.4807	.3319	.2679	.1869	.1842	.2856	.4928	.6736
750	.4812	.3341	.2836	.1822	.1847	.2916	.4931	.6774
760	.4807	.3357	.3004	.1876	.1848	.2991	.4940	.6811
770	.4805	.3371	.3210	.1840	.1842	.3075	.4947	.6860
780	.4804	.3392	.3446	.1913	.1838	.3175	.4961	.6920
790	.4779	.3381	.3672	.1979	.1834	.3294	.4978	.6988
800	.4751	.3369	.3891	.1927	.1824	.3412	.5002	.7025
810	.4731	.3342	.4077	.1861	.1809	.3534	.5044	.7106
820	.4714	.3323	.4242	.180	.1797	.3653	.5092	.7188
830	.4694	.3293	.4393	.1712	.1795	.3766	.5139	.7254
840	.4680	.3279	.4513	.1742	.1807	.3873	.5186	.7310
850	.4660	.3256	.4624	.1778	.1831	.3989	.5237	.7356
860	.4645	.3241	.4711	.1817	.1866	.4094	.5286	.7390
870	.4629	.3227	.4779	.1861	.1916	.4205	.5340	.7414
880	.4615	.3213	.4833	.1905	.1972	.4313	.5396	.7433
890	.4598	.3193	.4877	.1937	.2018	.4410	.5446	.7451
900	.4581	.3174	.4911	.1971	.2069	.4509	.5499	.7466
910	.4568	.3160	.4936	.2009	.2127	.4603	.5551	.7476
920	.4557	.3148	.4971	.2044	.2177	.4693	.5600	.7491
930	.4543	.3136	.5020	.2071	.2205	.4762	.5630	.7504
940	.4533	.3131	.5081	.2107	.2235	.4831	.5657	.7516
950	.4519	.3122	.5123	.2140	.2270	.4892	.5686	.7520
960	.4515	.3121	.5166	.2173	.2310	.4964	.5715	.7527
970	.4505	.3120	.5192	.221	.2340	.5029	.5740	.7517
980	.4503	.3142	.5245	.2235	.2419	.5093	.5761	.7503
990	.4498	.3183	.5287	.2329	.2471	.5163	.5780	.7499
1000	.4500	.3177	.5330	.2392	.2514	.5204	.5796	.7473
1010	.4502	.3201	.5371	.24	.2542	.5214	.5807	.7448
1020	.4502	.3222	.54	.24	.2562	.5221	.5820	.7417
1030	.4503	.325			.2728	.5279	.5833	.7391
1040	.4503	.3277			.2771	.5287	.5846	.7367

RECONSTRUCTED REFLECTANCE FUNCTIONS (ERROR) 3 COMPONENT

WAVELENGTH

WAVELENGTH	1	2	3	4	5	6	7	8
300	.0210	-.0275	.0263	-.0226	.0270	-.0223	.0267	-.0226
310	.0262	-.0387	.0373	-.0345	.0448	-.0417	.0333	-.0271
320	.0311	-.0436	.0505	-.0466	.0599	-.0565	.0453	-.0355
330	.0403	-.0552	.0637	-.0553	.0593	-.0703	.0759	-.0585
340	.0478	-.0568	.0731	-.0592	.0492	-.0793	.1079	-.0930
350	.0498	-.0490	.0752	-.0572	.0299	-.0797	.1337	-.1027
360	.0470	-.0369	.0698	-.0506	.0096	-.0716	.1436	-.1109
375	.0375	-.0210	.0519	-.0395	-.0032	-.0489	.1158	-.0927
400	.0255	-.0063	.0309	-.0265	-.0109	-.0237	.0757	-.0647
425	.0067	.0032	.0115	-.0107	-.0087	-.0080	.0339	-.0280
450	-.0027	.0070	.0020	-.0032	-.0068	-.0012	.0145	-.0105
475	-.0083	.0120	-.0019	.0013	-.0002	.0020	.0047	-.0014
500	-.0122	.0166	-.0037	-.0026	-.0033	.0045	.0003	.0025
525	-.0135	.0168	-.0053	-.0005	-.0055	.0070	-.0032	.0065
550	-.0129	.0181	-.0061	-.0014	-.0065	.0093	-.0048	.0043
575	-.0126	.0207	-.0069	-.0020	-.0049	.0120	-.0073	.0065
600	-.0103	.0206	-.0077	-.0051	-.0066	.0152	-.0107	.0047
625	-.0089	.0219	-.0080	-.0061	-.0076	.0191	-.0149	.0049
650	-.0065	.0216	-.0106	-.0064	-.0071	.0232	-.0217	.0073
675	-.0049	.0197	-.0119	-.0075	-.0047	.0257	-.0232	.0011
700	-.0037	.0162	-.0132	-.0048	-.0011	.0261	-.0237	.0162
725	-.0029	.0114	-.0147	-.0015	.0022	.0252	-.0410	.0017
750	-.0027	.0055	-.0171	.0030	.0131	.0261	-.0474	.0035
775	-.0030	-.0007	-.0190	.0132	.0033	.0213	-.0500	.0038
800	-.0030	-.0068	-.0211	.0222	.0034	.0184	-.0527	.0094
825	-.0036	-.0126	-.0231	.0204	.0034	.0154	-.0542	.0448
850	-.0054	-.0154	-.0265	.0357	.0037	.0131	-.0560	.0429
875	-.0069	-.0170	-.0246	.0334	.0039	.0107	-.0549	.0504
900	-.0081	-.0184	-.0241	.0408	.0034	.0078	-.0516	.0503
925	-.0119	-.0168	-.0229	.0409	.0035	.0042	-.0464	.0494
950	-.0167	-.0132	-.0216	.0398	.0037	.0013	-.0414	.0482
975	-.0199	-.0122	-.0193	.0389	.0053	-.0027	-.0357	.0466
1000	-.0224	-.0122	-.0167	.0361	.0078	-.0078	-.0298	.0446
1025	-.0222	-.0137	-.0117	.0310	.0126	-.0102	-.0235	.0430
1050	-.0198	-.0160	-.0067	.0216	.0177	-.0195	-.0157	.0341
1075	-.0171	-.0182	.0022	.0137	.0259	-.0236	-.0076	.0271
1100	-.0144	-.0177	.0079	.0059	.0304	-.0298	-.0010	.0233
1125	-.0116	-.0201	.0110	.0101	.0321	-.0216	.0046	.0166
1150	-.0104	.0031	.0031	.0066	.0320	-.0210	.0094	.0073
1175	-.0099	-.0153	.0117	-.0035	.0310	-.0409	.012	.0082
1200	-.0043	-.0177	.0161	.0021	.0321	-.0315	.0127	.0020
1225	-.0020	-.0157	.019	.0030	.0334	-.0310	.0116	-.0012
1250	-.0040	.0031	.00	-.0229	.0301	-.0164	.0081	-.0066
1275	.0035	.0077	.00	-.0077	.0301	-.0310	.0067	-.0077
1300	.0021	.0089	.00	.00	.0301	-.0310	.0067	-.0077
1325	.0021	.0089	.00	.00	.0319	.0004	.0004	.0004
1350	.0061	.0014	.0014	-.0031	.0301	.0015	.0015	.0015
1375	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027
1400	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027
1425	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027
1450	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027
1475	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027
1500	.0071	.0030	.0030	.0030	.0301	.0027	.0015	.0027

RECONSTRUCTED REFLECTANCE FUNCTIONAL (ERROR): 3 COMPONENT
(CONTINUED)

WAVELENGTH

	1	2	3	4	5	6	7	8
610	.0336	.0006	.0049	-.0321	-.0132	.0214	.0002	-.0286
615	.0240	-.0012	.0015	-.0127	-.0075	.0161	-.0037	-.0169
620	.0128	-.0009	-.0028	-.0027	-.0052	.0125	-.0096	-.0039
625	.0036	-.0013	-.0067	.0050	-.0022	.0095	-.0161	.0081
630	-.0056	.0000	-.0112	.0131	-.0015	.0083	-.0222	.0191
635	-.0114	.0011	-.0144	.0188	-.0021	.0077	-.0235	.0257
640	-.0165	.0023	-.0165	.0231	-.0023	.0066	-.0268	.0303
645	-.0196	.0037	-.0181	.0256	-.0035	.0062	-.0280	.0331
650	-.0229	.0050	-.0193	.0270	-.0040	.0062	-.0284	.0355
655	-.0247	.0054	-.0200	.0277	-.0047	.0056	-.0281	.0368
660	-.0255	.0052	-.0201	.0307	-.0050	.0048	-.0273	.0371
665	-.0262	.0042	-.0197	.0314	-.0053	.0039	-.0273	.0382
670	-.0259	.0032	-.0193	.0310	-.0029	.0024	-.0267	.0381
675	-.0259	.0013	-.0184	.0316	-.0013	.0003	-.0253	.0383
680	-.0257	-.0009	-.0169	.0311	.0011	-.0026	-.0245	.0384
685	-.0242	-.0041	-.0148	.0298	.0043	-.0056	-.0231	.0376
690	-.0227	-.0063	-.0124	.0274	.0072	-.0081	-.0210	.0369
695	-.0203	-.0091	-.0090	.0240	.0109	-.0115	-.0177	.0330
700	-.0184	-.0112	-.0046	.0187	.0152	-.0155	-.0131	.0290
705	-.0149	-.0116	.0012	.0132	-.0166	-.0164	-.0088	.0232
710	-.0111	-.0104	.0019	.0073	-.0166	-.0162	-.0042	.0165
715	-.0081	-.0092	.0043	.0010	.0171	-.0184	-.0014	.0114
720	-.0054	-.0082	.0062	-.0026	.0163	-.0143	.0010	.0062
725	-.0034	-.0050	.0077	-.0072	.0135	-.0126	.0042	.0016
730	-.0020	-.0039	.0087	-.0102	.0140	-.0113	.0064	-.0020
735	.0000	-.0026	.0096	-.0128	.0127	-.0099	.0083	-.0056
740	.0025	-.0021	.0099	-.0137	.0104	-.0084	.0104	-.0090
745	.0041	-.0017	.0101	-.0141	.0084	-.0075	.0120	-.0114
750	.0055	-.0013	.0097	-.0135	.0058	-.0063	.0134	-.0133
755	.0072	-.0013	.0093	-.0127	.0032	-.0050	.0144	-.0151
760	.0087	-.0014	.0089	-.0121	.0011	-.0039	.0151	-.0166
765	.0102	-.0010	.0084	-.0119	-.0007	-.0023	.0149	-.0176
770	.0113	.0002	.0079	-.0124	-.0027	-.0003	.0150	-.0191
775	.0127	.0004	.0080	-.0131	-.0035	.0008	.0150	-.0204
780	.0137	.0009	.0079	-.0137	-.0045	.0019	.0153	-.0216
785	.0151	.0008	.0077	-.0140	-.0050	.0031	.0144	-.0220
790	.0155	.0006	.0074	-.0138	-.0050	.0036	.0135	-.0217
795	.0155	-.0006	.0071	-.0131	-.0050	.0031	.0130	-.0207
800	.0157	-.0022	.0065	-.0120	-.0047	.0017	.0119	-.0193
805	.0162	-.0033	.0063	-.0089	-.0046	.0017	.0110	-.0179
810	.0160	-.0042	.0060	-.0040	-.0043	.0011	.0108	-.0163
815	.0161	-.0051	.0057	-.0007	-.0042	-.0014	.0092	-.0138
820	.0148	-.0119	.0050	-.0037	-.0042	-.0053	.0080	-.0107
825	.0127	-.0147	.0048	.0007	-.0041	-.0077	.0077	-.0081
830	.0132	-.0170	.0044	.0037	-.0040	-.0071	.0072	-.0057

RECONSTRUCTED CIE/CPI REFLECTANCE FUNCTIONS: 7 COMPONENT

Wavelength (nm)	1	2	3	4	5	6	7	8
400	.1160	.0830	.0580	.0570	.1430	.0799	.1500	.0750
410	.1360	.0550	.0590	.0590	.1870	.0810	.1770	.0730
420	.1590	.0590	.0610	.0620	.2330	.0890	.2180	.0840
430	.1900	.0640	.0630	.0670	.2690	.1130	.2930	.0900
440	.2190	.0700	.0650	.0740	.2950	.1510	.3780	.1040
450	.2390	.0720	.0680	.0880	.3040	.2031	.4590	.1290
460	.2520	.0887	.0699	.0930	.3130	.2651	.5241	.1700
470	.2560	.1010	.0720	.1050	.3120	.3390	.5460	.2400
480	.2560	.1110	.0730	.1160	.3130	.4100	.5510	.3190
490	.2540	.1140	.0730	.1210	.3150	.4640	.5530	.4160
500	.2520	.1150	.0740	.1240	.3190	.4920	.5590	.4620
510	.2480	.1200	.0740	.1260	.3200	.5080	.5600	.4920
520	.2440	.1210	.0740	.1280	.3260	.5170	.5610	.4990
530	.2400	.1220	.0730	.1311	.3200	.5240	.5570	.4970
540	.2370	.1220	.0730	.1341	.3240	.5310	.5580	.4910
550	.2320	.1220	.0730	.1391	.3290	.5380	.5500	.4720
560	.2300	.1210	.0730	.1441	.3480	.5430	.5430	.4610
570	.2260	.1240	.0730	.1490	.3320	.5500	.5340	.4470
580	.2250	.1270	.0740	.1540	.3600	.5560	.5220	.4390
590	.2220	.1380	.0750	.1600	.3690	.5560	.5060	.4260
600	.2200	.1310	.0770	.1670	.3810	.5500	.4880	.4160
610	.2180	.1240	.0800	.1730	.3940	.5490	.4670	.3970
620	.2160	.1380	.0810	.1790	.4060	.5411	.4420	.3730
630	.2140	.1430	.0940	.1840	.4100	.5310	.4290	.3660
640	.2140	.1500	.1090	.1810	.4150	.5190	.4081	.3621
650	.2140	.1589	.1250	.1807	.4180	.5041	.3851	.3671
660	.2160	.1730	.1470	.1819	.4190	.4881	.3631	.3631
670	.2180	.1990	.1710	.1819	.4170	.4691	.3411	.3601
680	.2230	.2060	.1970	.1860	.4130	.4501	.3241	.3591
690	.2250	.2240	.2200	.1820	.4090	.4311	.3111	.3591
700	.2260	.2410	.2400	.1800	.4030	.4141	.3011	.3580
710	.2260	.2530	.2600	.1840	.3960	.3950	.2910	.3560
720	.2250	.2600	.2760	.1980	.3890	.3770	.2830	.3560
730	.2250	.2640	.3000	.1920	.3810	.3580	.2730	.3520
740	.2270	.2670	.3390	.1950	.3720	.3410	.2650	.3540
750	.2300	.2690	.3780	.1970	.3630	.3250	.2600	.3510
760	.2360	.2720	.3920	.1970	.3570	.3090	.2570	.3500
770	.2470	.2741	.3990	.1970	.3510	.2970	.2570	.3510
780	.2530	.2720	.4000	.1970	.3410	.2810	.2590	.3540
790	.2610	.2690	.3930	.1970	.3340	.2660	.2600	.3590
800	.2720	.2690	.3810	.1970	.3280	.2500	.2630	.3630
810	.2810	.2690	.3690	.1970	.3220	.2340	.2630	.3630
820	.2900	.2690	.3570	.1970	.3160	.2180	.2630	.3630
830	.2990	.2690	.3450	.1970	.3100	.2020	.2630	.3630
840	.3080	.2690	.3330	.1970	.3040	.1860	.2630	.3630
850	.3170	.2690	.3210	.1970	.2980	.1700	.2630	.3630
860	.3260	.2690	.3090	.1970	.2920	.1540	.2630	.3630
870	.3350	.2690	.2970	.1970	.2860	.1380	.2630	.3630
880	.3440	.2690	.2850	.1970	.2800	.1220	.2630	.3630
890	.3530	.2690	.2730	.1970	.2740	.1060	.2630	.3630
900	.3620	.2690	.2610	.1970	.2680	.0900	.2630	.3630
910	.3710	.2690	.2490	.1970	.2620	.0740	.2630	.3630
920	.3800	.2690	.2370	.1970	.2560	.0580	.2630	.3630
930	.3890	.2690	.2250	.1970	.2500	.0420	.2630	.3630
940	.3980	.2690	.2130	.1970	.2440	.0260	.2630	.3630
950	.4070	.2690	.2010	.1970	.2380	.0100	.2630	.3630
960	.4160	.2690	.1890	.1970	.2320	.0040	.2630	.3630
970	.4250	.2690	.1770	.1970	.2260	.0000	.2630	.3630
980	.4340	.2690	.1650	.1970	.2200	.0000	.2630	.3630
990	.4430	.2690	.1530	.1970	.2140	.0000	.2630	.3630
1000	.4520	.2690	.1410	.1970	.2080	.0000	.2630	.3630

RECONSTRUCTION OF OFPI PERFORMANCE FUNCTIONS: 7 COMPONENT
(CONTINUED)

W/ALPHATH

	1	2	3	4	5	6	7	8
640	.4420	.3420	.2520	.1600	.1940	.2200	.3441	.6341
645	.4430	.3430	.2470	.1630	.1950	.2200	.3440	.6321
650	.44500	.3440	.2410	.1600	.1880	.2230	.3470	.6280
655	.44510	.3370	.2350	.1560	.1830	.2270	.3490	.6260
660	.44510	.3370	.2290	.1540	.1800	.2330	.34000	.6040
665	.44510	.3350	.2240	.1520	.1770	.2390	.34100	.6290
670	.44510	.3350	.2200	.1510	.1740	.2440	.34200	.6480
675	.44510	.3370	.2170	.1490	.1750	.2410	.34290	.6430
680	.44500	.3340	.2140	.1480	.1750	.2380	.3430	.6760
685	.44500	.3350	.2140	.1480	.1750	.2430	.3450	.6850
690	.44510	.3340	.2130	.1470	.1730	.2480	.3430	.6930
695	.44510	.337	.2090	.1450	.1730	.2530	.3430	.7000
700	.44530	.3370	.2000	.1450	.1800	.2580	.3430	.7040
705	.44540	.3370	.2380	.1540	.1830	.2610	.3430	.7090
710	.44550	.3310	.2510	.1520	.1840	.2630	.3430	.7120
715	.4470	.3370	.2490	.1520	.1870	.2640	.3400	.7150
720	.4480	.3270	.2890	.1600	.1920	.2610	.3430	.7170
725	.4490	.3270	.3120	.1600	.1950	.2650	.3470	.7190
730	.44620	.3220	.3400	.1700	.1990	.3020	.3430	.7210
735	.44630	.3270	.3440	.1710	.2000	.3130	.3490	.7300
740	.44640	.3240	.3900	.1740	.1990	.3250	.3460	.7190
745	.44650	.3270	.4120	.1830	.1950	.3300	.3500	.7210
750	.44660	.3240	.4310	.1840	.1940	.3510	.3110	.7290
755	.44660	.3240	.4470	.1840	.1950	.3640	.3180	.7270
760	.44660	.3240	.4600	.1840	.1950	.3760	.3250	.7290
765	.44660	.3230	.4720	.1850	.1960	.3890	.3320	.7300
770	.44670	.3220	.4810	.1880	.1970	.4010	.3390	.7300
775	.44670	.3210	.4890	.1720	.2000	.4130	.3460	.7300
780	.44670	.3200	.4930	.1770	.2030	.4250	.3530	.7300
785	.44670	.3180	.4970	.1810	.2050	.4360	.3590	.7300
790	.44670	.3160	.5000	.1850	.2080	.4470	.3650	.7300
795	.44670	.3150	.5020	.1890	.2120	.4580	.3700	.7300
800	.44670	.3150	.5050	.1920	.2130	.4690	.3750	.7300
805	.44670	.3140	.5100	.1940	.2170	.4770	.3780	.7300
810	.44670	.3140	.5160	.1970	.2190	.4850	.3810	.7300
815	.44670	.3130	.5200	.2000	.2220	.4930	.3830	.7300
820	.44670	.3130	.5240	.2040	.2230	.5000	.3850	.7310
825	.44660	.3120	.5270	.2070	.2310	.5040	.3870	.7310
830	.44660	.3120	.5310	.2110	.2370	.5130	.3900	.7310
835	.44660	.3110	.5350	.2150	.2430	.5170	.3990	.7310
840	.44660	.3100	.5370	.2180	.2490	.5240	.3990	.7310
845	.44660	.3100	.5400	.2210	.2570	.5280	.3990	.7310
850	.44650	.3100	.5420	.2240	.2630	.5370	.3990	.7311
855	.44650	.3100	.5440	.2270	.2710	.5420	.3990	.7311
860	.44640	.3100	.5460	.2300	.2780	.5480	.3990	.7311

RECONSTRUCTED REFLECTANCE FUNCTIONS (ERROR: 7 COMPONENT)

[illegible]

DATA MEAN AND COMPONENTS 1 - 7

STEP	INPUT	1	2	3	4	5	6	7
(10)	MEAN							
300	.0914	.0236	.0592	.0111	.0433	.0272	.0138	.0075
305	.1040	.0208	.0799	.0207	.0850	.0164	.0322	.0183
310	.1206	.0238	.1068	.0809	.1139	.0598	.0407	.0026
315	.1436	.0428	.1467	.0993	.1572	.0613	.0302	.0057
320	.1695	.0735	.1925	.1106	.1941	.0540	.0104	.0079
325	.1957	.1134	.2370	.1095	.2195	.0367	-.0159	.0118
330	.2216	.1593	.2779	.0998	.2178	.0185	-.0378	.0120
335	.2464	.2091	.3065	.0787	.1705	-.0020	-.0339	.0087
340	.2686	.2591	.3231	.0554	.1090	-.0154	-.0203	.0046
400	.2892	.3232	.3405	.0375	.0439	-.0113	-.0176	-.0025
410	.3000	.3530	.3496	.0277	.0139	-.0083	-.0125	-.0069
420	.3050	.3646	.3514	.0215	-.0019	-.0087	-.0100	-.0110
430	.3076	.367	.3624	.0177	-.0078	-.0074	-.0090	-.0114
440	.3082	.3627	.3682	.0140	-.0147	-.0094	-.0075	-.0142
450	.3087	.3546	.3747	.0113	-.0177	-.0127	-.0066	-.0163
460	.3084	.3431	.3817	.0068	-.0173	-.0155	-.0045	-.0174
470	.3092	.3235	.3874	.0045	-.0181	-.0170	-.0001	-.0172
480	.3077	.3116	.3933	.0006	-.0228	-.0230	.0002	-.0167
490	.3080	.2915	.3953	-.0012	-.0297	-.0253	.0063	-.0147
500	.3067	.2681	.3961	-.0027	-.0345	-.0242	.0146	-.0124
510	.3062	.2409	.3947	-.0026	-.0411	-.0206	.0213	-.0101
520	.3057	.2081	.3920	-.0019	-.0479	-.0147	.0240	-.0052
530	.3052	.1739	.3890	-.0002	-.0549	-.0078	.0265	.0011
540	.3051	.1387	.3727	.0044	-.0631	-.0006	.0250	.0073
550	.3060	.1029	.3548	-.0090	-.0697	.0073	.0231	.0153
560	.3064	.0655	.3317	-.0177	-.0759	.0150	.0208	.0221
570	.3081	.0309	.3024	-.0187	-.0806	.0205	.0183	.0342
580	.3086	-.0034	.2695	-.0242	-.0813	.0241	.0158	.0258
590	.3105	-.0317	.2347	-.0293	-.0794	.0273	.0120	.0268
600	.3117	-.0557	.2028	-.0328	-.0760	.0300	.0069	.0229
610	.3125	-.0717	.1736	-.0357	-.0726	.0311	.0021	.0168
620	.3114	-.0853	.1453	-.0399	-.0670	.0345	-.0014	.0126
630	.3096	-.0952	.1212	-.0455	-.0601	.0390	-.0041	.0087
640	.3071	-.1047	.0932	-.0552	-.0490	.0435	-.0030	.0054
650	.3065	-.1109	.0594	-.0753	-.0319	.0480	.0014	.0009
660	.3056	-.1186	.0304	-.0910	-.0152	.0513	.0049	-.0026
670	.3045	-.1106	.0029	-.0921	-.0011	.0524	.0077	-.0052
680	.3021	-.1017	-.0184	-.0941	.0101	.0520	.0092	-.0047
690	.2999	-.0901	-.0302	-.0930	.0201	.0499	.0086	-.0092
700	.2967	-.0747	-.0465	-.0917	.0281	.0463	.0095	-.0125
710	.2935	-.0543	-.0585	-.0916	.0287	.0422	.0095	-.0162
720	.2896	-.0307	-.0699	-.0919	.0289	.0381	.0101	-.0193
730	.2849	-.0046	-.0804	-.0927	.0287	.0339	.0104	-.0212
740	.2835	.0077	-.0897	-.0935	.0281	.0297	.0093	-.0259
750	.284	.0157	-.0977	-.0941	.0271	.0255	.0087	-.0313
760	.2807	.0247	-.1047	-.0945	.0257	.0213	.0077	-.0367
770	.2810	.0347	-.1107	-.0947	.0239	.0171	.0062	-.0417
780	.2823	.0452	-.1157	-.0945	.0217	.0129	.0050	-.0467
790	.2869	.0569	-.1197	-.0939	.0187	.0087	.0041	-.0519
800	.2922	.0697	-.1227	-.0929	.0151	.0051	.0034	-.0569

3.00 HEAR AND COMPONENTS 1 - 7
 (CONTINUED)

WAVELENGTH		COMPONENT						
WAVELENGTH		1	2	3	4	5	6	7
690	.32998	.1211	-.1241	.1251	.0269	-.0409	.0205	.0143
700	.33068	.1212	-.1273	.1324	.0133	-.0273	.0154	.0122
710	.33131	.1253	-.1279	.1377	-.0033	-.0137	.0106	.0099
720	.33195	.1300	-.1282	.1414	-.0189	-.0048	.0083	.0074
730	.33257	.1304	-.1239	.1445	-.0347	.0032	.0044	.0047
740	.33319	.1353	.1202	.1453	-.0448	.0067	.0007	.0034
750	.33380	.1404	-.1140	.1476	-.0514	.0103	-.0032	.0017
760	.33440	.1443	-.1103	.1494	-.0567	.0112	-.0034	.0005
770	.33501	.1429	-.1080	.1487	-.0592	.0129	-.0022	-.0011
780	.33576	.1416	-.1013	.1442	-.0617	.0141	-.0104	-.0013
790	.34225	.1467	-.0990	.1409	-.0618	.0150	-.0119	-.0014
800	.3454	.1483	-.0962	.1384	-.0621	.0176	-.0119	-.0013
810	.3489	.1477	-.0936	.1316	-.0610	.0109	-.0115	-.0010
820	.3520	.1457	-.0939	.1249	-.0596	.0222	-.0114	-.0004
830	.3555	.1473	-.1000	.1174	-.0567	.0239	-.0106	-.0002
840	.3597	.149	-.1052	.1071	-.0523	.0249	-.0094	.0003
850	.3641	.1497	-.1103	.0989	-.0469	.0326	-.0063	.0000
860	.3694	.1498	-.1172	.0937	-.0390	.0357	-.0037	.0002
870	.3752	.1471	-.1247	.0842	-.0294	.0383	-.0008	-.0009
880	.3811	.1434	-.1238	.0721	-.0181	.0366	.0015	-.0017
890	.3861	.1425	-.1318	.0616	-.0093	.0322	.0031	-.0028
900	.3914	.1402	-.1341	-.0022	-.0010	.0292	.0054	-.0043
910	.3962	.1312	-.1351	-.0241	.0059	.0235	.0046	-.0054
920	.4004	.1242	-.1344	-.0139	.0115	.0182	.0074	-.0076
930	.4049	.1162	-.1323	-.0080	.0157	.0141	.0074	-.0032
940	.4091	.1081	-.1284	-.0050	.0197	.0097	.0076	-.0091
950	.4131	.1009	-.1236	-.0032	.0239	.0058	.0065	-.0076
960	.4171	.1034	-.1169	-.0070	.0253	.0029	.0054	-.0066
970	.4210	.1047	-.1039	-.0044	.0265	-.0001	.0035	-.0049
980	.4241	.1048	-.1016	-.1013	.0275	-.0030	.0021	-.0027
990	.4272	.1047	-.0933	-.1074	.0282	-.0055	.0010	-.0007
1000	.4304	.1038	-.0849	-.1122	.0280	-.0082	.0007	.0007
1010	.4335	.1036	-.0777	-.1177	.0283	-.0118	.0003	.0011
1020	.4359	.1029	-.0737	-.1240	.0292	-.0133	.0009	.0018
1030	.4386	.1014	-.0706	-.1307	.0300	-.0159	.0009	.0022
1040	.4410	.1000	-.0661	-.1362	.0299	-.0175	.0019	.0032
1050	.4437	.1000	-.0622	-.1408	.0290	-.0178	.0024	.0032
1060	.4462	.1004	-.0571	-.1463	.0275	-.0164	.0023	.0051
1070	.4488	.1003	-.0531	-.1487	.0260	-.0147	.0023	.0071
1080	.4521	.1002	-.0492	-.1534	.0249	-.0123	.0022	.0091
1090	.4550	.1000	-.0462	-.1587	.0235	-.0094	.0025	.0107
1100	.4584	.1000	-.0432	-.1642	.0215	-.0071	.0020	.0131
1110	.4616	.1000	-.0392	-.1697	.0171	-.0095	.0022	.0153
1120	.4647	.1000	-.0349	-.1751	.0121	-.0044	.0017	.0169
1130	.4678	.1000	-.0321	-.1807	.0077	-.0092	.0004	.0201

a correlated color temperature of 6800 K and the CIE illuminant C as a reference was 80. Subsequent papers have shown an improvement of this figure to 94 when the three component distribution was combined with a continuous spectrum.³

Many questions have arisen concerning the adequateness of the original CIE set of eight color test samples for measurement of the general CRI. Nayatani et. al. showed that because of deficiencies in the number and choice of the test samples involved it is possible to derive, for a given reference illuminant, an infinite number of test illuminants with a different SPD that all have perfect color rendering indices.⁴ In agreeing with this view Dr. Wyszecki, of the National Research Council of Canada, has suggested the use of metameric gray object colors generated statistically so as to be non-linearly related in assessing the color matching properties of lamps.^{5,6} Nayatani and Takahama have confirmed the effectiveness of using the twelve metameric grays derived by Dr. Wyszecki in making an assessment of this type.⁷

Although the use of properly chosen line spectra can provide a wide gamut of colors these same spectra could be disastrous in reproducing certain colors. Since the CRI was shown to increase even more when combined SPDs were used it would be beneficial to know if the maximum of the three line spectra could be accounted for by an interrelationship in the test samples. If the samples are interrelated and can be represented by three functions it is highly probable that these three functions would be the cause of maximization of CRI at wavelengths of 450, 540, and 610 nm. Determination of the